



Cokenergy LLC

3210 Watling Street MC 2-991
East Chicago, IN 46312

October 17, 2018

Chief, Environmental Enforcement Section
Environment and Natural Resources Division
U.S. Department of Justice
Box 7611, Ben Franklin Station
Washington, DC 20044-7611
Re: DOJ No. 90-5-2-1-08555/1

Air Enforcement Division Director
U.S. Environmental Protection Agency
Office of Civil Enforcement
Air Enforcement Division
U.S. Environmental Protection Agency
1200 Pennsylvania Ave, NW Mail Code: 2242A
Washington, DC 20460

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100 North Senate Avenue
MC-61-53, IGCN 1003
Indianapolis, IN 46204-2251

Elizabeth A. Zlatos
Indiana Department of Environmental Management
Office of Legal Counsel
100 North Senate Avenue
MC-60-01, IGCN 1307
Indianapolis, IN 46204-2251

RE: Consent Decree, *United States, et. al. v. Indiana Harbor Coke Company, et. al.*
Cokenergy, LLC (Part 70 Permit No. T089-36965-00383)
Cokenergy Flow Monitor Initial Certification and Relative Accuracy Test Audit Report

To Whom It May Concern:

Pursuant to the proposed Consent Decree (CD) entered in federal court on August 13, 2018, Cokenergy is submitting this Relative Accuracy Test Audit (RATA) report for the volumetric flow monitoring system installed on the Cokenergy main stack (Stack 201) in accordance with CD paragraph 19. The RATA was completed on September 12, 2018 and the 7-day calibration drift test was completed between September 8 and September 14, 2018.

The results from the calibration drift test ranged from 0% to 0.4%, well within the $\leq 3\%$ of span standard. The RATA results for the flow monitor were 6.40% and 4.09% for the sulfur dioxide (SO₂) emission rate, both well within the $\leq 20\%$ standard from the applicable performance specification.

I certify under penalty of law that this information was prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my directions and inquiry of the person(s) who manage the system, or the person(s) directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties



for submitting false information, including the possibility of fine and imprisonment for knowing violations.

If you have any questions, please contact me at (219) 397-4626.

Sincerely,

A handwritten signature in black ink, appearing to read "Luke E. Ford", written in a cursive style.

Luke E. Ford
Director EH&S

cc: East Chicago Public Libraries

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2401 E. Columbus Drive
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**CONTINUOUS EMISSIONS MONITORING SYSTEM RELATIVE ACCURACY
DETERMINATION AND CERTIFICATION TEST**

Performed At

**Primary Energy
Cokenergy Facility
HRCC Stack 201
East Chicago, Indiana**

Test Dates

**September 12, 2018 (RATA)
September 8 through 14, 2018 (Calibration Drift testing)**

Report No.

TRC Environmental Corporation Report 305091

Report Submittal Date

October 15, 2018

TRC Environmental Corporation
7521 Brush Hill Road
Burr Ridge, Illinois 60527
USA

T 312-533-2042
F 312-533-2070



Report Certification

I certify that to the best of my knowledge:

- Testing data and all corresponding information have been checked for accuracy and completeness.
- Sampling and analysis have been conducted in accordance with the approved protocol and applicable reference methods (as applicable).
- All deviations, method modifications, or sampling and analytical anomalies are summarized in the appropriate report narrative(s).

A handwritten signature in black ink, appearing to read 'Gavin Lewis', is written over a thin horizontal line.

Gavin Lewis
Project Manager

October 15, 2018

Date

TRC was operating in conformance with the requirements of ASTM D7036-04 during this test program.

A handwritten signature in black ink, appearing to read 'BRR', is written over a thin horizontal line.

Bruce Randall
TRC Emission Testing Technical Director



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**CONTINUOUS EMISSIONS MONITORING SYSTEM RELATIVE ACCURACY
DETERMINATION AND CERTIFICATION TEST**

1.0 INTRODUCTION

Cokenergy installed a volumetric flow monitoring system as part of their existing Continuous Emissions Monitoring System (CEMS) on the HRCC Stack 201.

The purpose of this test program was to certify the HRCC Stack 201 CEMS. TRC Environmental Corporation (TRC) performed the relative accuracies tests on September 12, 2018 while the unit was operating at greater than 50% of normal load. Primary Energy personnel performed the seven-day calibration drift tests on September 8 through 14. All tests were performed in accordance with methods described in the Code of Federal Regulations, Title 40, Part 60 (40CFR60), Appendix B, Performance Specifications 2 and 3. The test program was conducted according to the Indiana Department of Environmental Management (IDEM) Relative Accuracy Test Audit Notification Protocol dated August 1, 2018.

1.1 Project Contact Information

| Participants | | |
|---|---|---|
| Test Facility | Primary Energy Cokenergy Facility East Chicago, Indiana | Mr. Luke Ford Director EH&S 219-397-4626 (phone) lford@primaryenergy.com |
| Test Coordinator | Primary Energy 3210 Watling Street East Chicago, Indiana 46312 Permit No. T089-36965-00383 | |
| Air Emissions Testing Body (AETB) | TRC Environmental Corporation 7521 Brush Hill Road Burr Ridge, Illinois 60527 | Mr. Gavin Lewis Project Manager 312-533-2025 (phone) 312-533-2070 (fax) glewis@trcsolutions.com |

William Manny, Ryan Novosel and Gavin Lewis of TRC conducted the testing. Documentation of the on-site ASTM D7036-04 Qualified Individual(s) (QI) can be located in the appendix to this report.

No personnel from the IDEM observed the testing.



2.0 SUMMARY OF RESULTS

The results of these tests are presented in the following tables. Tables 2.1 and 2.2 present a summary of the actual performance of each component of the CEMS system, as compared to United States Environmental Protection Agency (USEPA) 40 CFR Part 60 specifications.

Table 2.1 – Gaseous Results

| Load | Parameter | Units | Performance Specifications (40CFR60) | | CEMS Performance |
|-------|-----------------|-------|--------------------------------------|--|-------------------|
| | | | Specification No. | Acceptance Criteria | Relative Accuracy |
| > 50% | SO ₂ | ppmvd | 2 | RA ≤ 20% of the Reference Method | 2.68 % |
| > 50% | SO ₂ | lb/hr | 2 | RA ≤ 20% of the Reference Method | 4.09 % |
| > 50% | O ₂ | % dry | 3 | RA ≤ 1.0% difference for %O ₂ | 0.20 %vol diff |

Table 2.2 – Volumetric Flowrate, Performance Specification 6

| Serial Number: 031518-000-1118-UMCR | | Span: 0 – 1,000 kscfm | |
|-------------------------------------|---------------------|---|--------------------|
| Criteria | Test Date(s) | Required Performance | Actual Performance |
| Calibration Error | 09/08/18 – 09/14/18 | ≤ 3.0% of high level value for each of 7 days | ≤ 0.4 % |
| Relative Accuracy | 09/12/18 | RA ≤ 20% of the Reference Method (dscfm) | 6.40 % |



3.0 DISCUSSION OF RESULTS

The complete test results from this program are tabulated in Section 6.0.

The data acquisition and handling system (DAHS) computer printout for the same time periods as the RM testing was used to determine the relative accuracy. The watches of the test crew were synchronized with the CEMS prior to testing.

No problems were encountered with the testing equipment during the course of the test program. Source operation appeared normal during the entire test program and operated at more than 50 percent of full load. The CEMS operation appeared normal with no apparent problems during sampling. No changes or problems were encountered that required modification of any procedures presented in the test plan. No adverse test or environmental conditions were encountered during the conduct of this test program. CEMS operating data was recorded by plant personnel and appended to the report.

4.0 TEST PROCEDURES

All testing, sampling, analytical, and calibration procedures used for this test program were performed in accordance with the methods presented in the following sections. Where applicable, the Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III, Stationary Source Specific Methods, USEPA 600/R-94/038c, September 1994 was used to supplement procedures.

4.1 Calibration Drift Test

Calibration Drift tests were performed by Primary Energy personnel. A summary of the test data is presented in Section 6.1 and supporting documentation is appended to the report.

4.2 Relative Accuracy Tests

4.2.1 CEMS RATA Test Matrix

| Parameter | Reference Methods (RM) | No. of Test Runs | Test Run Length (min) |
|---|----------------------------|------------------|-----------------------|
| SO ₂ | 6C (1, 2, 3A, 4 for lb/hr) | 10 | 21 |
| O ₂ (CO ₂ for flow only) | 3A | 10 | 21 |
| Flow | 1, 2 and 4 | 10 | ≥ 5 |

4.2.2 Determination of Sample Point Locations by USEPA Method 1

This method is applicable to gas streams flowing in ducts, stacks, and flues and is designed to aid in the representative measurement of pollutant emissions and/or total volumetric flow rates from stationary sources. In order to qualify as an acceptable sample location, it must be located at a position at least two stack or duct equivalent diameters downstream and a half equivalent diameter upstream from any flow disturbance.

The cross-section of the measurement site was divided into a number of equal areas, and the traverse points were then located in the center of these areas. The minimum number of points were determined from Figure 1-2 (non-particulate) of USEPA Method 1.

4.2.3 Volumetric Flow Rate Determination by USEPA Method 2

This method is applicable for the determination of the average velocity and the volumetric flow rate of a gas stream.

The gas velocity head (ΔP) and temperature were measured at traverse points defined by USEPA Method 1. The velocity head was measured with a Type S (Stausscheibe or reverse type) pitot tube and oil-filled manometer; and the gas temperature was measured with a Type K thermocouple. The average gas velocity in the flue was calculated based on: the gas density (as determined by USEPA Methods 3 and 4); the flue gas pressure; the average of the square roots of the velocity heads at each traverse point, and the average flue gas temperature.

4.2.4 Determination of the Concentration of Gaseous Pollutants Using a Multi-Pollutant Sampling System

Concentrations of the pollutants in the following sub-sections were determined using one sampling system. The number of points at which sample was collected was determined in accordance with 40CFR60 specifications.

A straight-extractive sampling system was used. Gas samples were collected for seven (7) minutes at each of three points (0.4, 1.2 and 2.0 meters) along the stack diameter during each test run. A data logger continuously recorded pollutant concentrations and generated one-minute averages of those concentrations. All calibrations and system checks were conducted using USEPA Protocol gases. Three-point linearity checks were performed prior to sampling, and in the event of a failing system bias or drift test (and subsequent corrective action). System bias and drift checks were performed using the low-level gas and either the mid- or high-level gas prior to and following each test run.



The Low Concentration Analyzers (those that routinely operate with a calibration span of less than 20 ppm) used by TRC are ambient-level analyzers. Per Section 3.12 of Method 7E, a Manufacturer's Stability Test is not required for ambient-level analyzers. Analyzer interference tests were conducted in accordance with the regulations in effect at the time that TRC placed an analyzer model in service.

4.2.4.1 CO₂ Determination by USEPA Method 3A

This method is applicable for the determination of carbon dioxide (CO₂) concentrations in controlled and uncontrolled emissions from stationary sources only when specified within the regulations. The CO₂ analyzer was equipped with a non-dispersive infrared (IR) detector.

4.2.4.2 O₂ Determination by USEPA Method 3A

This method is applicable for the determination of O₂ concentrations in controlled and uncontrolled emissions from stationary sources only when specified within the regulations. The O₂ analyzer was equipped with a paramagnetic-based detector.

4.2.4.3 SO₂ Determination by USEPA Method 6C

This method is applicable for the determination of SO₂ concentrations in controlled and uncontrolled emissions from stationary sources only when specified within the regulations. The SO₂ analyzer was equipped with an ultraviolet (UV) detector.

4.2.5 Moisture Determination by USEPA Method 4

This method is applicable for the determination of the moisture content of stack gas.

A gas sample was extracted at a constant rate from the source. Moisture was removed from the sample stream by a series of pre-weighed impingers immersed in an ice bath. A minimum of 21 dry standard cubic feet of flue gas was collected during each sample run.



5.0 QUALITY ASSURANCE PROCEDURES

TRC integrates our Quality Management System (QMS) into every aspect of our testing service. We follow the procedures specified in current published versions of the test Method(s) referenced in this report. Any modifications or deviations are specifically identified in the body of the report. We routinely participate in independent, third party audits of our activities, and maintain:

- Accreditation from the Louisiana Environmental Laboratory Accreditation Program (LELAP);
- Accreditation from the Stack Testing Accreditation Council (STAC) and the American Association for Laboratory Accreditation (A2LA) that our operations conform with the requirements of ASTM D 7036 as an Air Emission Testing Body (AETB).

These accreditations demonstrate that our systems for training, equipment maintenance and calibration, document control and project management will fully ensure that project objectives are achieved in a timely and efficient manner with a strict commitment to quality.

All calibrations are performed in accordance with the test Method(s) identified in this report. If a Method allows for more than one calibration approach, or if approved alternatives are available, the calibration documentation in the appendices specifies which approach was used. All measurement devices are calibrated or verified at set intervals against standards traceable to the National Institute of Standards and Technology (NIST). NIST traceability information is available upon request.

ASTM D7036-04 specifies that: *“AETBs shall have and shall apply procedures for estimating the uncertainty of measurement. Conformance with this section may be demonstrated by the use of approved test protocols for all tests. When such protocols are used, reference shall be made to published literature, when available, where estimates of uncertainty for test methods may be found.”* TRC conforms with this section by using approved test protocols for all tests.



6.0 TEST RESULTS SUMMARIES



6.1 Calibration Drift Test Results Summary

Owner: Primary Energy
Plant: Cokenergy Facility
Source ID: HRCC Stack 201

CEM Component: Volumetric Flow
Instrument Span: 0 - 1,000 kscfm
Test Dates: 09/08/18 - 09/14/18
Certification Criteria: 40 CFR 60, Appendix B

| Day | Load Level | Date | Time | Reference Value | CEM Value | Difference | Calibration Error % |
|-----|------------|----------|---------|-----------------|-----------|------------|---------------------|
| 1 | Zero | 09/08/18 | 5:33:10 | 0.00 | 3.00 | 3.00 | 0.3 |
| 2 | Zero | 09/09/18 | 5:33:09 | 0.00 | 2.00 | 2.00 | 0.2 |
| 3 | Zero | 09/10/18 | 5:33:14 | 0.00 | 3.90 | 3.90 | 0.4 |
| 4 | Zero | 09/11/18 | 5:33:12 | 0.00 | 3.70 | 3.70 | 0.4 |
| 5 | Zero | 09/12/18 | 5:33:12 | 0.00 | 3.90 | 3.90 | 0.4 |
| 6 | Zero | 09/13/18 | 5:33:12 | 0.00 | 3.70 | 3.70 | 0.4 |
| 7 | Zero | 09/14/18 | 5:33:11 | 0.00 | 3.60 | 3.60 | 0.4 |
| 1 | Span | 09/08/18 | 5:36:10 | 750.00 | 749.50 | 0.50 | 0.1 |
| 2 | Span | 09/09/18 | 5:36:08 | 750.00 | 749.20 | 0.80 | 0.1 |
| 3 | Span | 09/10/18 | 5:36:15 | 750.00 | 750.30 | 0.30 | 0.0 |
| 4 | Span | 09/11/18 | 5:36:14 | 750.00 | 750.10 | 0.10 | 0.0 |
| 5 | Span | 09/12/18 | 5:36:13 | 750.00 | 750.10 | 0.10 | 0.0 |
| 6 | Span | 09/13/18 | 5:36:12 | 750.00 | 750.00 | 0.00 | 0.0 |
| 7 | Span | 09/14/18 | 5:36:13 | 750.00 | 750.00 | 0.00 | 0.0 |

Drift Specification: Flow CEM: $\leq 3\%$ of span maximum



6.2 Relative Accuracy Summaries



RATA Type: Sulfur Dioxide (SO₂), ppm
Regulation: 40CFR60
RM Used: 6C

| Customer: | | Primary Energy | | | Project #: | | 305091 | |
|------------------------|----------|----------------|------------|----------|--------------------------|---------------------------|--------------------------|--|
| Unit ID: | | HRCC | | | CEM Model: | | Thermo Scientific 43i-HL | |
| Sample Loc: | | Stack 201 | | | CEM Serial #: | | 1152150034 | |
| Use? 1 = Y 0 = N | Test Run | Date | Start Time | End Time | RM SO ₂ ppmvd | CEM SO ₂ ppmvd | (RM-CEM) Difference (di) | |
| 1 | 1 | 9/12/18 | 7:15 | 7:35 | 155.5 | 160.1 | -4.6 | |
| 1 | 2 | 9/12/18 | 8:00 | 8:20 | 151.7 | 154.3 | -2.6 | |
| 1 | 3 | 9/12/18 | 8:40 | 9:00 | 155.5 | 158.0 | -2.5 | |
| 1 | 4 | 9/12/18 | 9:20 | 9:40 | 144.9 | 148.6 | -3.7 | |
| 0 | 5 | 9/12/18 | 10:00 | 10:20 | 139.3 | 143.9 | -4.6 | |
| 1 | 6 | 9/12/18 | 10:45 | 11:05 | 132.6 | 135.5 | -2.9 | |
| 1 | 7 | 9/12/18 | 11:25 | 11:45 | 134.6 | 138.7 | -4.1 | |
| 1 | 8 | 9/12/18 | 12:05 | 12:25 | 135.1 | 138.2 | -3.1 | |
| 1 | 9 | 9/12/18 | 12:45 | 13:05 | 128.3 | 130.4 | -2.1 | |
| 1 | 10 | 9/12/18 | 13:25 | 13:45 | 123.3 | 125.3 | -2.0 | |

| | | |
|------------------------|---------|---------|
| n | 9 | |
| t(0.975) | 2.306 | |
| Mean RM Value | 140.167 | RM avg |
| Mean CEM Value | 143.233 | CEM avg |
| Mean Difference | -3.067 | d avg |
| Standard Deviation | 0.899 | sd |
| Confidence Coefficient | 0.691 | CC |
| RA based on RM | 2.68 | % |



RATA Type: Sulfur Dioxide (SO₂), lb/hr
Regulation: 40CFR60
RM Used: 2-4, 6C

| Customer: | | Primary Energy | | | Project #: | | 305091 | |
|------------------------|-------------|----------------|---------------|-------------|--------------------------------|---------------------------------|--------------------------------|--|
| Unit ID: | | HRCC | | | CEM Model: | | Thermo Scientific 43i-HL | |
| Sample Loc: | | Stack 201 | | | CEM Serial #: | | 1152150034 | |
| Use? 1 = Y 0 = N | Test Run | Date | Start Time | End Time | RM SO ₂ lb/hr | CEM SO ₂ lb/hr | (RM-CEM) Difference (di) | |
| 1 | 1 | 9/12/18 | 7:15 | 7:35 | 995.5 | 953.3 | 42.2 | |
| 0 | 2 | 9/12/18 | 8:00 | 8:20 | 985.6 | 915.4 | 70.2 | |
| 1 | 3 | 9/12/18 | 8:40 | 9:00 | 978.4 | 935.2 | 43.2 | |
| 1 | 4 | 9/12/18 | 9:20 | 9:40 | 899.6 | 873.7 | 25.9 | |
| 1 | 5 | 9/12/18 | 10:00 | 10:20 | 867.5 | 854.9 | 12.6 | |
| 1 | 6 | 9/12/18 | 10:45 | 11:05 | 837.5 | 805.9 | 31.6 | |
| 1 | 7 | 9/12/18 | 11:25 | 11:45 | 844.0 | 825.2 | 18.8 | |
| 1 | 8 | 9/12/18 | 12:05 | 12:25 | 855.6 | 826.7 | 28.9 | |
| 1 | 9 | 9/12/18 | 12:45 | 13:05 | 807.9 | 781.9 | 26.0 | |
| 1 | 10 | 9/12/18 | 13:25 | 13:45 | 760.6 | 738.5 | 22.1 | |

| | | |
|------------------------|---------|---------|
| n | 9 | |
| t(0.975) | 2.306 | |
| Mean RM Value | 871.844 | RM avg |
| Mean CEM Value | 843.922 | CEM avg |
| Mean Difference | 27.922 | d avg |
| Standard Deviation | 10.071 | sd |
| Confidence Coefficient | 7.741 | CC |
| RA based on RM | 4.09 | % |



RATA Type: Oxygen (O₂), % by volume
Regulation: 40CFR60
RM Used: 3A

| Customer: | | Primary Energy | | | Project #: | | 305091 | |
|------------------------|-------------|----------------|---------------|-------------|-----------------------------------|------------------------------------|--------------------------------|--|
| Unit ID: | | HRCC | | | CEM Model: | | Brand Gaus 4705 | |
| Sample Loc: | | Stack 201 | | | CEM Serial #: | | 11401 | |
| Use? 1 = Y 0 = N | Test Run | Date | Start Time | End Time | RM O ₂ % v/v dry | CEM O ₂ % v/v dry | (RM-CEM) Difference (di) | |
| 1 | 1 | 9/12/18 | 7:15 | 7:35 | 12.6 | 12.8 | -0.2 | |
| 1 | 2 | 9/12/18 | 8:00 | 8:20 | 12.7 | 12.9 | -0.2 | |
| 1 | 3 | 9/12/18 | 8:40 | 9:00 | 12.8 | 13.0 | -0.2 | |
| 1 | 4 | 9/12/18 | 9:20 | 9:40 | 13.0 | 13.2 | -0.2 | |
| 1 | 5 | 9/12/18 | 10:00 | 10:20 | 13.0 | 13.2 | -0.2 | |
| 1 | 6 | 9/12/18 | 10:45 | 11:05 | 13.1 | 13.3 | -0.2 | |
| 1 | 7 | 9/12/18 | 11:25 | 11:45 | 13.2 | 13.4 | -0.2 | |
| 1 | 8 | 9/12/18 | 12:05 | 12:25 | 13.4 | 13.6 | -0.2 | |
| 1 | 9 | 9/12/18 | 12:45 | 13:05 | 13.5 | 13.7 | -0.2 | |
| 0 | 10 | 9/12/18 | 13:25 | 13:45 | 13.5 | 13.7 | -0.2 | |

| | | |
|-------------------------------|--------|-------------|
| n | 9 | |
| t(0.975) | 2.306 | |
| Mean RM Value | 13.033 | RM avg |
| Mean CEM Value | 13.233 | CEM avg |
| Mean Difference | -0.200 | d avg |
| Standard Deviation | 0.000 | sd |
| Confidence Coefficient | 0.000 | CC |
| RA (Absolute Mean Difference) | 0.20 | % vol diff. |



RATA Type: Flow, (DSCFM)*, High Load

Regulation: 40CFR60

RM Used: 2

| | | | |
|-----------|-------------------------------------|---------------|----------------------|
| Customer: | Primary Energy - Cokenergy Facility | Project #: | 305091 |
| Unit ID: | HRCC | CEM Model: | -- |
| Location: | Stack 201 | CEM Serial #: | 031518-000-1118-UMCR |

| Use? 1 = Y 0 = N | Test Run | Date | Start Time | End Time | RM Volumetric Flow (DSCFM)* | CEM Volumetric Flow (DSCFM)* | (RM-CEM) Difference (di) |
|------------------------|-------------|-----------|---------------|-------------|-----------------------------------|------------------------------------|--------------------------------|
| 1 | 1 | 9/12/2018 | 07:15 | 07:25 | 643,000 | 598,000 | 45,000 |
| 0 | 2 | 9/12/2018 | 08:00 | 08:08 | 652,000 | 597,000 | 55,000 |
| 1 | 3 | 9/12/2018 | 08:40 | 08:49 | 632,000 | 592,000 | 40,000 |
| 1 | 4 | 9/12/2018 | 09:20 | 09:28 | 623,000 | 580,000 | 43,000 |
| 1 | 5 | 9/12/2018 | 10:00 | 10:10 | 625,000 | 597,000 | 28,000 |
| 1 | 6 | 9/12/2018 | 10:45 | 10:54 | 634,000 | 598,000 | 36,000 |
| 1 | 7 | 9/12/2018 | 11:25 | 11:33 | 630,000 | 599,000 | 31,000 |
| 1 | 8 | 9/12/2018 | 12:05 | 12:13 | 636,000 | 599,000 | 37,000 |
| 1 | 9 | 9/12/2018 | 12:45 | 12:53 | 632,000 | 601,000 | 31,000 |
| 1 | 10 | 9/12/2018 | 13:25 | 13:33 | 619,000 | 590,000 | 29,000 |

| | |
|------------------------|---------------------|
| n | 9 |
| t(0.975) | 2.306 |
| Mean RM Value | 630,444.444 RM avg |
| Mean CEM Value | 594,888.889 CEM avg |
| Mean Difference | 35,555.556 d avg |
| Standard Deviation | 6,207.075 sd |
| Confidence Coefficient | 4,771.172 CC |
| Relative Accuracy | 6.40 % RA |

*Standard conditions of 29.92 in/Hg and 68° F

APPENDIX

AETB and QI Information Summary

| | |
|-----------------------|-------------------------------------|
| Facility Name: | Primary Energy – Cokenergy Facility |
| Location: | HRCC Stack 201 |
| Test Date: | September 12, 2018 (RATA) |



| | |
|---------------------------|--|
| Test Parameters: | 1, 2, 3A, 4, 6C |
| QI Last Name: | Lewis |
| QI First Name: | Gavin |
| QI Middle Initial: | ---- |
| AETB Name: | TRC Environmental Corporation |
| AETB Phone No: | 312-533-2025 |
| AETB Email: | glewis@trcsolutions.com |
| Group 1 Exam Date: | 11/07/2017 |
| Provider Name: | Source Evaluation Society |
| Provider Email: | gstiprogram@gmail.com |
| Group 3 Exam Date: | 01/05/2018 |
| Provider Name: | Source Evaluation Society |
| Provider Email: | gstiprogram@gmail.com |

This is to Certify that:

Gavin Lewis

Is a Qualified Individual as defined in Section 8.3 of ASTM D7036-04 for the following test methods:

EPA Methods 1, 1A, 2, 2A, 2C, 2D, 2F, 2G, 2H, 3, 3B, 4, 5, 5A, 5B, 5D, 5E, 5F, 5i, 17, 19, 201A, and 202.

The individual has met the minimum experience requirements defined in Section 8.3.4.2 of ASTM D7036-04 and has successfully passed a comprehensive examination for the test methods designated above.

This certification is effective until: 11/07/2022

Date of Issue: 01-08-2018

Certificate Number: 01249



Edward J MacKinnon
Air Measurements Practice Quality Manager



This certificate is the exclusive property of TRC and is non-transferable.

This is to Certify that:

Gavin Lewis

Is a Qualified Individual as defined in Section 8.3 of ASTM D7036-04 for the following test methods:

EPA Methods 3A, 6C, 7E, 10, 10B, 19, 20, 25A.

CEM Performance Specifications PS2, PS3, PS4, PS4A, PS5, PS6, PS7, PS8, and PS15

The individual has met the minimum experience requirements defined in Section 8.3.4.2 of ASTM D7036-04 and has successfully passed a comprehensive examination for the test methods designated above.

This certification is effective until: 01-05-2023

Date of Issue: 01-08-2018

Certificate Number: 01251



Edward J. MacKinnon

Edward J MacKinnon
Air Measurements Practice Quality Manager

This certificate is the exclusive property of TRC and is non-transferable.

Calibration Report

09/08/2018 - 09/14/2018

| Date | Timestamp | Parameter | Type | Measured | Expected | Error | Tolerance | Result |
|------------|-----------|-----------------|------|----------|----------|-------|-----------|--------|
| 09/08/2018 | 05:33:10 | VOL FLOW, KSCFM | Zero | 3.0 | 0.0 | 0.3 | 3 | Pass |
| | 05:36:10 | VOL FLOW, KSCFM | Span | 749.5 | 750.0 | 0.1 | 3 | Pass |
| 09/09/2018 | 05:33:09 | VOL FLOW, KSCFM | Zero | 2.0 | 0.0 | 0.2 | 3 | Pass |
| | 05:36:08 | VOL FLOW, KSCFM | Span | 749.2 | 750.0 | 0.1 | 3 | Pass |
| 09/10/2018 | 05:33:14 | VOL FLOW, KSCFM | Zero | 3.9 | 0.0 | 0.4 | 3 | Pass |
| | 05:36:15 | VOL FLOW, KSCFM | Span | 750.3 | 750.0 | 0.0 | 3 | Pass |
| 09/11/2018 | 05:33:12 | VOL FLOW, KSCFM | Zero | 3.7 | 0.0 | 0.4 | 3 | Pass |
| | 05:36:14 | VOL FLOW, KSCFM | Span | 750.1 | 750.0 | 0.0 | 3 | Pass |
| 09/12/2018 | 05:33:13 | VOL FLOW, KSCFM | Zero | 3.9 | 0.0 | 0.4 | 3 | Pass |
| | 05:36:13 | VOL FLOW, KSCFM | Span | 750.1 | 750.0 | 0.0 | 3 | Pass |
| 09/13/2018 | 05:33:12 | VOL FLOW, KSCFM | Zero | 3.7 | 0.0 | 0.4 | 3 | Pass |
| | 05:36:12 | VOL FLOW, KSCFM | Span | 750.0 | 750.0 | 0.0 | 3 | Pass |
| 09/14/2018 | 05:33:11 | VOL FLOW, KSCFM | Zero | 3.6 | 0.0 | 0.4 | 3 | Pass |
| | 05:36:13 | VOL FLOW, KSCFM | Span | 750.0 | 750.0 | 0.0 | 3 | Pass |

RATA Data Report

East Chicago, IN


9/12/2018 7:15:00 AM - 9/12/2018 7:35:00 AM

STACK 201

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 07:15:00 | 164.8 | 12.8 | 11.0 | 11.7 | 982.1 |
| 07:16:00 | 162.6 | 12.8 | 11.0 | 11.7 | 965.2 |
| 07:17:00 | 165.0 | 12.8 | 11.0 | 11.7 | 984.7 |
| 07:18:00 | 166.2 | 12.8 | 11.0 | 11.7 | 992.2 |
| 07:19:00 | 163.5 | 12.8 | 11.0 | 11.7 | 978.9 |
| 07:20:00 | 161.7 | 12.8 | 11.0 | 11.7 | 958.4 |
| 07:21:00 | 159.4 | 12.8 | 11.0 | 11.7 | 949.9 |
| 07:22:00 | 157.9 | 12.8 | 11.0 | 11.7 | 937.5 |
| 07:23:00 | 158.7 | 12.8 | 11.0 | 11.7 | 942.1 |
| 07:24:00 | 159.0 | 12.8 | 11.0 | 11.7 | 947.8 |
| 07:25:00 | 158.3 | 12.8 | 11.0 | 11.7 | 949.0 |
| 07:26:00 | 158.8 | 12.8 | 11.0 | 11.7 | 933.2 |
| 07:27:00 | 158.8 | 12.8 | 11.0 | 11.7 | 954.1 |
| 07:28:00 | 157.9 | 12.8 | 11.0 | 11.7 | 951.5 |
| 07:29:00 | 157.9 | 12.8 | 11.0 | 11.7 | 937.8 |
| 07:30:00 | 159.7 | 12.8 | 11.0 | 11.7 | 938.1 |
| 07:31:00 | 158.5 | 12.8 | 11.0 | 11.7 | 947.0 |
| 07:32:00 | 158.4 | 12.8 | 11.0 | 11.7 | 954.3 |
| 07:33:00 | 160.1 | 12.8 | 11.0 | 11.7 | 942.9 |
| 07:34:00 | 157.1 | 12.8 | 11.0 | 11.7 | 929.9 |
| 07:35:00 | 158.0 | 12.8 | 11.0 | 11.7 | 942.3 |
| Average : | 160.1 | 12.8 | 11.0 | 11.7 | 953.3 |

* Invalid Status

RATA Run # 1

Verified By: 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 08:00:00 | 154.1 | 12.9 | 11.1 | 11.6 | 928.1 |
| 08:01:00 | 154.0 | 12.9 | 11.1 | 11.6 | 904.8 |
| 08:02:00 | 156.3 | 12.9 | 11.1 | 11.6 | 923.9 |
| 08:03:00 | 155.5 | 12.9 | 11.1 | 11.6 | 927.3 |
| 08:04:00 | 154.0 | 12.9 | 11.1 | 11.6 | 915.4 |
| 08:05:00 | 154.0 | 12.9 | 11.1 | 11.6 | 915.9 |
| 08:06:00 | 155.0 | 12.9 | 11.1 | 11.6 | 921.6 |
| 08:07:00 | 153.1 | 12.9 | 11.1 | 11.6 | 898.2 |
| 08:08:00 | 154.6 | 12.9 | 11.1 | 11.6 | 927.7 |
| 08:09:00 | 151.6 | 12.9 | 11.1 | 11.6 | 899.8 |
| 08:10:00 | 152.5 | 12.9 | 11.1 | 11.6 | 907.5 |
| 08:11:00 | 151.1 | 12.9 | 11.1 | 11.6 | 895.1 |
| 08:12:00 | 154.5 | 12.9 | 11.1 | 11.6 | 926.2 |
| 08:13:00 | 153.8 | 12.9 | 11.1 | 11.6 | 919.7 |
| 08:14:00 | 153.8 | 12.9 | 11.1 | 11.6 | 911.0 |
| 08:15:00 | 153.4 | 12.9 | 11.1 | 11.6 | 905.4 |
| 08:16:00 | 153.7 | 12.9 | 11.1 | 11.6 | 908.9 |
| 08:17:00 | 154.3 | 12.9 | 11.1 | 11.6 | 917.5 |
| 08:18:00 | 156.2 | 12.9 | 11.1 | 11.6 | 910.1 |
| 08:19:00 | 157.5 | 12.9 | 11.1 | 11.6 | 930.7 |
| 08:20:00 | 157.5 | 12.9 | 11.1 | 11.6 | 929.3 |
| Average : | 154.3 | 12.9 | 11.1 | 11.6 | 915.4 |

* Invalid Status

RATA Run # 2


Verified By:

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 08:40:00 | 156.6 | 13.0 | 11.2 | 11.5 | 924.5 |
| 08:41:00 | 156.2 | 12.9 | 11.2 | 10.9 | 919.0 |
| 08:42:00 | 157.7 | 13.0 | 11.2 | 11.5 | 942.4 |
| 08:43:00 | 157.2 | 13.0 | 11.1 | 12.3 | 921.1 |
| 08:44:00 | 159.4 | 13.0 | 11.2 | 11.5 | 944.0 |
| 08:45:00 | 159.4 | 13.0 | 11.2 | 11.5 | 942.1 |
| 08:46:00 | 159.5 | 13.0 | 11.2 | 11.5 | 940.8 |
| 08:47:00 | 160.7 | 13.0 | 11.2 | 11.5 | 950.4 |
| 08:48:00 | 159.3 | 13.0 | 11.2 | 11.5 | 928.2 |
| 08:49:00 | 160.4 | 13.0 | 11.2 | 11.5 | 948.3 |
| 08:50:00 | 159.9 | 13.0 | 11.2 | 11.5 | 952.2 |
| 08:51:00 | 156.4 | 13.0 | 11.2 | 11.5 | 932.6 |
| 08:52:00 | 157.8 | 13.0 | 11.2 | 11.5 | 930.6 |
| 08:53:00 | 156.6 | 13.0 | 11.2 | 11.5 | 927.9 |
| 08:54:00 | 156.5 | 13.0 | 11.2 | 11.5 | 928.2 |
| 08:55:00 | 157.4 | 13.0 | 11.2 | 11.5 | 941.2 |
| 08:56:00 | 155.8 | 13.0 | 11.2 | 11.5 | 919.0 |
| 08:57:00 | 157.9 | 13.0 | 11.2 | 11.5 | 936.1 |
| 08:58:00 | 158.5 | 13.0 | 11.2 | 11.5 | 949.9 |
| 08:59:00 | 157.4 | 13.0 | 11.2 | 11.5 | 927.5 |
| 09:00:00 | 156.9 | 13.1 | 11.2 | 12.2 | 933.1 |
| Average : | 158.0 | 13.0 | 11.2 | 11.5 | 935.2 |

* Invalid Status


RATA Run # 3

Verified By: 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 09:20:00 | 139.3 | 13.3 | 11.5 | 11.3 | 795.1 |
| 09:21:00 | 142.0 | 13.3 | 11.5 | 11.3 | 791.3 |
| 09:22:00 | 142.5 | 13.3 | 11.5 | 11.3 | 795.8 |
| 09:23:00 | 142.2 | 13.3 | 11.5 | 11.3 | 839.4 |
| 09:24:00 | 143.6 | 13.3 | 11.5 | 11.3 | 834.1 |
| 09:25:00 | 145.8 | 13.2 | 11.4 | 11.4 | 847.8 |
| 09:26:00 | 148.3 | 13.2 | 11.4 | 11.4 | 878.4 |
| 09:27:00 | 149.9 | 13.2 | 11.4 | 11.4 | 876.8 |
| 09:28:00 | 151.9 | 13.2 | 11.4 | 11.4 | 891.1 |
| 09:29:00 | 151.7 | 13.1 | 11.4 | 10.7 | 900.5 |
| 09:30:00 | 152.4 | 13.2 | 11.4 | 11.4 | 895.6 |
| 09:31:00 | 153.4 | 13.2 | 11.4 | 11.4 | 907.6 |
| 09:32:00 | 151.2 | 13.2 | 11.4 | 11.4 | 894.5 |
| 09:33:00 | 153.0 | 13.2 | 11.4 | 11.4 | 909.5 |
| 09:34:00 | 153.1 | 13.1 | 11.4 | 10.7 | 918.1 |
| 09:35:00 | 150.3 | 13.2 | 11.4 | 11.4 | 893.0 |
| 09:36:00 | 150.3 | 13.1 | 11.3 | 11.5 | 876.6 |
| 09:37:00 | 150.2 | 13.2 | 11.4 | 11.4 | 897.4 |
| 09:38:00 | 150.1 | 13.1 | 11.4 | 10.7 | 908.7 |
| 09:39:00 | 151.1 | 13.2 | 11.4 | 11.4 | 897.7 |
| 09:40:00 | 149.3 | 13.1 | 11.3 | 11.5 | 898.9 |
| Average : | 148.6 | 13.2 | 11.4 | 11.3 | 873.7 |

* Invalid Status


RATA Run #4
Verified By: 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|-----------|----------|-----------|-----------|--------|------------|
| 10:00:00 | 145.5 | 13.2 | 11.4 | 11.4 | 863.4 |
| 10:01:00 | 143.8 | 13.1 | 11.4 | 10.7 | 854.6 |
| 10:02:00 | 143.1 | 13.2 | 11.4 | 11.4 | 857.2 |
| 10:03:00 | 143.1 | 13.2 | 11.4 | 11.4 | 860.7 |
| 10:04:00 | 145.4 | 13.2 | 11.4 | 11.4 | 865.1 |
| 10:05:00 | 144.9 | 13.2 | 11.4 | 11.4 | 860.7 |
| 10:06:00 | 144.5 | 13.2 | 11.4 | 11.4 | 852.7 |
| 10:07:00 | 146.2 | 13.2 | 11.4 | 11.4 | 877.9 |
| 10:08:00 | 145.4 | 13.2 | 11.4 | 11.4 | 854.3 |
| 10:09:00 | 147.1 | 13.2 | 11.4 | 11.4 | 878.6 |
| 10:10:00 | 146.1 | 13.2 | 11.4 | 11.4 | 855.2 |
| 10:11:00 | 148.1 | 13.2 | 11.4 | 11.4 | 875.8 |
| 10:12:00 | 143.9 | 13.2 | 11.4 | 11.4 | 859.9 |
| 10:13:00 | 142.1 | 13.2 | 11.4 | 11.4 | 853.2 |
| 10:14:00 | 143.2 | 13.2 | 11.4 | 11.4 | 849.6 |
| 10:15:00 | 141.4 | 13.2 | 11.4 | 11.4 | 832.5 |
| 10:16:00 | 142.9 | 13.2 | 11.4 | 11.4 | 855.7 |
| 10:17:00 | 141.8 | 13.2 | 11.4 | 11.4 | 830.3 |
| 10:18:00 | 142.9 | 13.2 | 11.4 | 11.4 | 849.1 |
| 10:19:00 | 141.7 | 13.2 | 11.4 | 11.4 | 847.2 |
| 10:20:00 | 139.2 | 13.2 | 11.4 | 11.4 | 818.3 |
| Average : | 143.9 | 13.2 | 11.4 | 11.4 | 854.9 |

* Invalid Status

RATA Run # 5


Verified By: 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 10:45:00 | 136.1 | 13.2 | 11.4 | 11.4 | 809.3 |
| 10:46:00 | 136.3 | 13.3 | 11.5 | 11.3 | 804.5 |
| 10:47:00 | 137.9 | 13.2 | 11.4 | 11.4 | 812.0 |
| 10:48:00 | 136.4 | 13.3 | 11.5 | 11.3 | 809.8 |
| 10:49:00 | 137.7 | 13.3 | 11.5 | 11.3 | 818.8 |
| 10:50:00 | 135.1 | 13.2 | 11.5 | 10.6 | 811.3 |
| 10:51:00 | 137.5 | 13.3 | 11.5 | 11.3 | 819.8 |
| 10:52:00 | 136.4 | 13.3 | 11.5 | 11.3 | 818.9 |
| 10:53:00 | 134.7 | 13.2 | 11.5 | 10.6 | 807.9 |
| 10:54:00 | 136.6 | 13.3 | 11.5 | 11.3 | 810.1 |
| 10:55:00 | 135.5 | 13.3 | 11.5 | 11.3 | 812.4 |
| 10:56:00 | 135.6 | 13.3 | 11.5 | 11.3 | 794.4 |
| 10:57:00 | 136.8 | 13.3 | 11.5 | 11.3 | 818.3 |
| 10:58:00 | 134.9 | 13.3 | 11.5 | 11.3 | 803.6 |
| 10:59:00 | 134.2 | 13.3 | 11.5 | 11.3 | 802.5 |
| 11:00:00 | 134.2 | 13.3 | 11.5 | 11.3 | 796.4 |
| 11:01:00 | 135.0 | 13.3 | 11.5 | 11.3 | 799.1 |
| 11:02:00 | 133.1 | 13.3 | 11.5 | 11.3 | 791.3 |
| 11:03:00 | 134.7 | 13.3 | 11.5 | 11.3 | 798.8 |
| 11:04:00 | 134.1 | 13.3 | 11.5 | 11.3 | 799.9 |
| 11:05:00 | 133.0 | 13.3 | 11.5 | 11.3 | 785.4 |
| Average : | 135.5 | 13.3 | 11.5 | 11.2 | 805.9 |

* Invalid Status

RATA Run # 6

Verified By: 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 11:25:00 | 135.8 | 13.3 | 11.6 | 10.5 | 819.9 |
| 11:26:00 | 135.6 | 13.4 | 11.6 | 11.2 | 804.7 |
| 11:27:00 | 137.4 | 13.4 | 11.6 | 11.2 | 816.4 |
| 11:28:00 | 136.4 | 13.4 | 11.6 | 11.2 | 816.5 |
| 11:29:00 | 138.4 | 13.4 | 11.6 | 11.2 | 820.0 |
| 11:30:00 | 137.6 | 13.4 | 11.6 | 11.2 | 816.5 |
| 11:31:00 | 137.8 | 13.4 | 11.6 | 11.2 | 829.7 |
| 11:32:00 | 137.8 | 13.4 | 11.6 | 11.2 | 813.5 |
| 11:33:00 | 138.0 | 13.4 | 11.6 | 11.2 | 825.5 |
| 11:34:00 | 136.5 | 13.4 | 11.6 | 11.2 | 811.9 |
| 11:35:00 | 138.3 | 13.4 | 11.6 | 11.2 | 813.9 |
| 11:36:00 | 138.1 | 13.4 | 11.6 | 11.2 | 818.3 |
| 11:37:00 | 139.4 | 13.4 | 11.6 | 11.2 | 832.8 |
| 11:38:00 | 139.7 | 13.4 | 11.6 | 11.2 | 829.1 |
| 11:39:00 | 139.6 | 13.4 | 11.6 | 11.2 | 822.6 |
| 11:40:00 | 140.9 | 13.4 | 11.6 | 11.2 | 843.1 |
| 11:41:00 | 139.4 | 13.4 | 11.6 | 11.2 | 826.3 |
| 11:42:00 | 140.7 | 13.4 | 11.7 | 10.4 | 834.5 |
| 11:43:00 | 140.5 | 13.4 | 11.7 | 10.4 | 835.3 |
| 11:44:00 | 141.2 | 13.4 | 11.7 | 10.4 | 844.8 |
| 11:45:00 | 143.0 | 13.5 | 11.7 | 11.1 | 853.1 |
| Average : | 138.7 | 13.4 | 11.6 | 11.0 | 825.2 |

* Invalid Status


RATA Run # 7
 Verified By 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 12:05:00 | 140.5 | 13.6 | 11.8 | 11.0 | 841.3 |
| 12:06:00 | 139.0 | 13.6 | 11.8 | 11.0 | 830.5 |
| 12:07:00 | 140.4 | 13.6 | 11.8 | 11.0 | 835.7 |
| 12:08:00 | 139.6 | 13.6 | 11.8 | 11.0 | 822.8 |
| 12:09:00 | 138.7 | 13.6 | 11.8 | 11.0 | 830.5 |
| 12:10:00 | 139.1 | 13.6 | 11.8 | 11.0 | 827.1 |
| 12:11:00 | 136.9 | 13.6 | 11.8 | 11.0 | 818.0 |
| 12:12:00 | 137.3 | 13.6 | 11.8 | 11.0 | 830.1 |
| 12:13:00 | 137.0 | 13.6 | 11.8 | 11.0 | 814.2 |
| 12:14:00 | 139.1 | 13.6 | 11.8 | 11.0 | 838.9 |
| 12:15:00 | 139.1 | 13.6 | 11.8 | 11.0 | 837.5 |
| 12:16:00 | 139.9 | 13.6 | 11.9 | 10.3 | 838.6 |
| 12:17:00 | 140.5 | 13.6 | 11.9 | 10.3 | 848.4 |
| 12:18:00 | 140.1 | 13.7 | 11.9 | 10.9 | 834.7 |
| 12:19:00 | 140.7 | 13.6 | 11.9 | 10.3 | 859.9 |
| 12:20:00 | 137.1 | 13.6 | 11.8 | 11.0 | 813.3 |
| 12:21:00 | 135.7 | 13.7 | 11.9 | 10.9 | 800.5 |
| 12:22:00 | 135.6 | 13.6 | 11.9 | 10.3 | 818.0 |
| 12:23:00 | 134.5 | 13.6 | 11.8 | 11.0 | 802.3 |
| 12:24:00 | 135.7 | 13.6 | 11.9 | 10.3 | 808.2 |
| 12:25:00 | 136.7 | 13.7 | 11.9 | 10.9 | 810.7 |
| Average : | 138.2 | 13.6 | 11.8 | 10.8 | 826.7 |

* Invalid Status

RATA Run #8

Verified By: 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 12:45:00 | 133.8 | 13.7 | 11.9 | 10.9 | 799.3 |
| 12:46:00 | 135.2 | 13.7 | 11.9 | 10.9 | 810.2 |
| 12:47:00 | 133.4 | 13.7 | 11.9 | 10.9 | 792.7 |
| 12:48:00 | 131.5 | 13.7 | 11.9 | 10.9 | 782.4 |
| 12:49:00 | 129.4 | 13.7 | 11.9 | 10.9 | 776.5 |
| 12:50:00 | 130.2 | 13.7 | 11.9 | 10.9 | 779.0 |
| 12:51:00 | 130.6 | 13.7 | 12.0 | 10.2 | 780.9 |
| 12:52:00 | 130.7 | 13.7 | 12.0 | 10.2 | 781.6 |
| 12:53:00 | 130.1 | 13.7 | 12.0 | 10.2 | 785.4 |
| 12:54:00 | 129.5 | 13.7 | 12.0 | 10.2 | 776.1 |
| 12:55:00 | 130.5 | 13.7 | 12.0 | 10.2 | 781.3 |
| 12:56:00 | 128.6 | 13.7 | 11.9 | 10.9 | 771.7 |
| 12:57:00 | 130.1 | 13.7 | 12.0 | 10.2 | 779.3 |
| 12:58:00 | 130.4 | 13.7 | 12.0 | 10.2 | 781.2 |
| 12:59:00 | 129.6 | 13.7 | 12.0 | 10.2 | 788.2 |
| 13:00:00 | 129.0 | 13.7 | 11.9 | 10.9 | 765.9 |
| 13:01:00 | 131.1 | 13.7 | 12.0 | 10.2 | 786.6 |
| 13:02:00 | 129.4 | 13.7 | 12.0 | 10.2 | 776.6 |
| 13:03:00 | 128.4 | 13.7 | 12.0 | 10.2 | 777.0 |
| 13:04:00 | 129.3 | 13.7 | 12.0 | 10.2 | 772.7 |
| 13:05:00 | 127.9 | 13.7 | 12.0 | 10.2 | 775.5 |
| Average : | 130.4 | 13.7 | 12.0 | 10.5 | 781.9 |

* Invalid Status

RATA Run # 9
 Verified By: 

RATA Data Report

| Time | SO2, PPM | O2 DRY, % | O2 WET, % | H2O, % | SO2, LB/HR |
|------------------|--------------|-------------|-------------|-------------|--------------|
| 13:25:00 | 128.4 | 13.7 | 11.9 | 10.9 | 747.9 |
| 13:26:00 | 125.6 | 13.7 | 11.9 | 10.9 | 726.3 |
| 13:27:00 | 123.7 | 13.7 | 11.9 | 10.9 | 730.1 |
| 13:28:00 | 123.7 | 13.7 | 11.9 | 10.9 | 735.9 |
| 13:29:00 | 124.3 | 13.7 | 11.9 | 10.9 | 726.1 |
| 13:30:00 | 124.6 | 13.7 | 11.9 | 10.9 | 733.9 |
| 13:31:00 | 121.5 | 13.7 | 11.9 | 10.9 | 716.6 |
| 13:32:00 | 123.0 | 13.7 | 11.9 | 10.9 | 725.0 |
| 13:33:00 | 137.7 | 13.7 | 11.9 | 10.9 | 813.7 |
| 13:34:00 | 139.8 | 13.7 | 11.9 | 10.9 | 830.3 |
| 13:35:00 | 136.2 | 13.7 | 11.9 | 10.9 | 804.0 |
| 13:36:00 | 121.5 | 13.7 | 12.0 | 10.2 | 720.6 |
| 13:37:00 | 121.0 | 13.7 | 11.9 | 10.9 | 712.0 |
| 13:38:00 | 121.6 | 13.7 | 12.0 | 10.2 | 715.4 |
| 13:39:00 | 123.4 | 13.7 | 12.0 | 10.2 | 736.8 |
| 13:40:00 | 122.6 | 13.7 | 12.0 | 10.2 | 720.9 |
| 13:41:00 | 123.1 | 13.7 | 12.0 | 10.2 | 729.5 |
| 13:42:00 | 121.8 | 13.7 | 12.0 | 10.2 | 719.3 |
| 13:43:00 | 122.9 | 13.7 | 12.0 | 10.2 | 719.9 |
| 13:44:00 | 123.4 | 13.8 | 12.0 | 10.9 | 724.5 |
| 13:45:00 | 122.0 | 13.7 | 12.0 | 10.2 | 719.7 |
| Average : | 125.3 | 13.7 | 11.9 | 10.6 | 738.5 |

* Invalid Status

RATA Run # 10

Verified By:



RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|--------------------|------------------------|
| 07:15:00 | 677.6 | 598.3 |
| 07:16:00 | 675.0 | 596.0 |
| 07:17:00 | 678.6 | 599.2 |
| 07:18:00 | 678.8 | 599.4 |
| 07:19:00 | 680.7 | 601.1 |
| 07:20:00 | 673.9 | 595.1 |
| 07:21:00 | 677.6 | 598.3 |
| 07:22:00 | 675.1 | 596.1 |
| 07:23:00 | 675.0 | 596.0 |
| 07:24:00 | 677.8 | 598.5 |
| 07:25:00 | 681.6 | 601.9 |

Average : 677.4 598.2

* Invalid Status

RATA Run # 1

Verified By:

RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|--------------------|------------------------|
| 08:00:00 | 684.0 | 604.7 |
| 08:01:00 | 667.3 | 589.9 |
| 08:02:00 | 671.4 | 593.5 |
| 08:03:00 | 677.3 | 598.7 |
| 08:04:00 | 675.1 | 596.8 |
| 08:05:00 | 675.4 | 597.1 |
| 08:06:00 | 675.3 | 597.0 |
| 08:07:00 | 666.3 | 589.0 |
| 08:08:00 | 681.6 | 602.5 |

Average : 674.9 596.6

* Invalid Status

RATA Run # 2
Verified By:




RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|-----------|--------------------|------------------------|
| 08:40:00 | 669.7 | 592.7 |
| 08:41:00 | 663.0 | 590.7 |
| 08:42:00 | 678.0 | 600.0 |
| 08:43:00 | 670.8 | 588.3 |
| 08:44:00 | 671.9 | 594.6 |
| 08:45:00 | 670.5 | 593.4 |
| 08:46:00 | 669.1 | 592.2 |
| 08:47:00 | 671.0 | 593.8 |
| 08:48:00 | 661.0 | 585.0 |
| 08:49:00 | 670.7 | 593.6 |
| Average : | 669.6 | 592.4 |

* Invalid Status

RATA Run # 3

Verified By: 

RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|-----------|--------------------|------------------------|
| 09:20:00 | 646.1 | 573.1 |
| 09:21:00 | 630.8 | 559.5 |
| 09:22:00 | 632.1 | 560.7 |
| 09:23:00 | 668.2 | 592.7 |
| 09:24:00 | 657.5 | 583.2 |
| 09:25:00 | 658.9 | 583.8 |
| 09:26:00 | 671.2 | 594.7 |
| 09:27:00 | 662.9 | 587.3 |
| 09:28:00 | 664.8 | 589.0 |
| Average : | 654.7 | 580.4 |

* Invalid Status

RATA Run # 4
 Verified By: 

RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|--------------------|------------------------|
| 10:00:00 | 672.5 | 596.8 |
| 10:01:00 | 668.2 | 596.7 |
| 10:02:00 | 678.8 | 601.4 |
| 10:03:00 | 681.6 | 603.9 |
| 10:04:00 | 674.3 | 597.4 |
| 10:05:00 | 673.1 | 596.4 |
| 10:06:00 | 668.7 | 592.5 |
| 10:07:00 | 680.5 | 602.9 |
| 10:08:00 | 665.8 | 589.9 |
| 10:09:00 | 676.9 | 599.7 |
| 10:10:00 | 663.3 | 587.7 |

Average : 673.1 596.8

* Invalid Status

RATA Run # 5
Verified By: 

RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|--------------------|------------------------|
| 10:45:00 | 673.8 | 597.0 |
| 10:46:00 | 668.1 | 592.6 |
| 10:47:00 | 667.3 | 591.2 |
| 10:48:00 | 672.0 | 596.1 |
| 10:49:00 | 673.1 | 597.0 |
| 10:50:00 | 674.4 | 602.9 |
| 10:51:00 | 674.9 | 598.6 |
| 10:52:00 | 679.6 | 602.8 |
| 10:53:00 | 673.6 | 602.2 |
| 10:54:00 | 671.2 | 595.4 |

Average : 672.8 597.6

* Invalid Status

RATA Run # 6

Verified By:




RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|--------------------|------------------------|
| 11:25:00 | 677.3 | 606.2 |
| 11:26:00 | 670.9 | 595.8 |
| 11:27:00 | 671.8 | 596.6 |
| 11:28:00 | 676.8 | 601.0 |
| 11:29:00 | 669.9 | 594.9 |
| 11:30:00 | 670.9 | 595.8 |
| 11:31:00 | 680.7 | 604.5 |
| 11:32:00 | 667.5 | 592.7 |
| 11:33:00 | 676.4 | 600.6 |

Average : 673.6 598.7

* Invalid Status

RATA Run # 7
Verified By: 

RATA Data Report

VOL FLOW, KSCFM VOL FLOW DRY, KSCFM

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|-----------------|---------------------|
| 12:05:00 | 675.5 | 601.2 |
| 12:06:00 | 674.0 | 599.9 |
| 12:07:00 | 671.5 | 597.6 |
| 12:08:00 | 664.9 | 591.8 |
| 12:09:00 | 675.5 | 601.2 |
| 12:10:00 | 670.8 | 597.0 |
| 12:11:00 | 674.1 | 599.9 |
| 12:12:00 | 682.0 | 607.0 |
| 12:13:00 | 670.4 | 596.7 |

Average : 673.2 599.1

* Invalid Status

RATA Run # 8

Verified By:



RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|--------------------|------------------------|
| 12:45:00 | 673.2 | 599.8 |
| 12:46:00 | 675.3 | 601.7 |
| 12:47:00 | 669.6 | 596.6 |
| 12:48:00 | 670.5 | 597.4 |
| 12:49:00 | 676.2 | 602.5 |
| 12:50:00 | 674.2 | 600.7 |
| 12:51:00 | 668.5 | 600.3 |
| 12:52:00 | 668.6 | 600.4 |
| 12:53:00 | 674.9 | 606.1 |

Average : 672.3 600.6

* Invalid Status

RATA Run # 9

Verified By:



RATA Data Report

| Time | VOL FLOW, KSCFM | VOL FLOW DRY, KSCFM |
|----------|--------------------|------------------------|
| 13:25:00 | 656.3 | 584.8 |
| 13:26:00 | 651.6 | 580.6 |
| 13:27:00 | 665.1 | 592.6 |
| 13:28:00 | 670.4 | 597.3 |
| 13:29:00 | 658.3 | 586.5 |
| 13:30:00 | 663.7 | 591.4 |
| 13:31:00 | 664.6 | 592.2 |
| 13:32:00 | 664.2 | 591.8 |
| 13:33:00 | 665.9 | 593.3 |

Average : 662.2 590.1

* Invalid Status

RATA Run # 10

Verified By:



Sample Location Information for Volumetric Flow Determination - Round Ducts

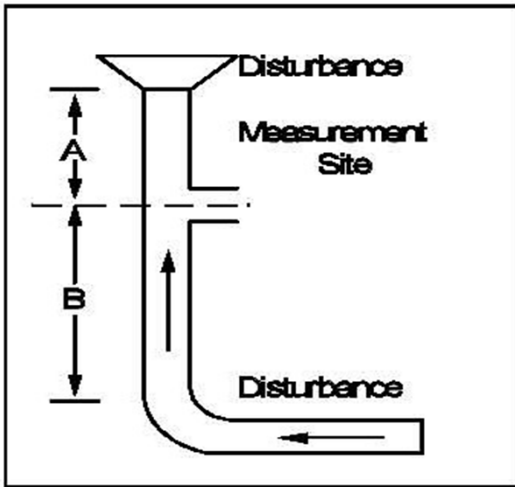
Project #: 305091
 Company: Primary Energy
 Plant: Cokenergy Facility
 Unit ID: HRCC
 Sample Location: Stack 201

Duct Diameter: 18.00 feet
 # of Ports Used: 4
 # of Points/Diameter: 8
 Total # of points: 16
 Sample Plane: Horizontal
 Port Type: Nipple
 Port Length: 7.0 inches
 Port Inside Diameter: 6.0 inches

Distance A: 73.80 Feet, 4.10 Duct diameters
 Distance B: 201.00 Feet, 11.17 Duct diameters

Meets Method 1 criteria

Traverse Point Locations

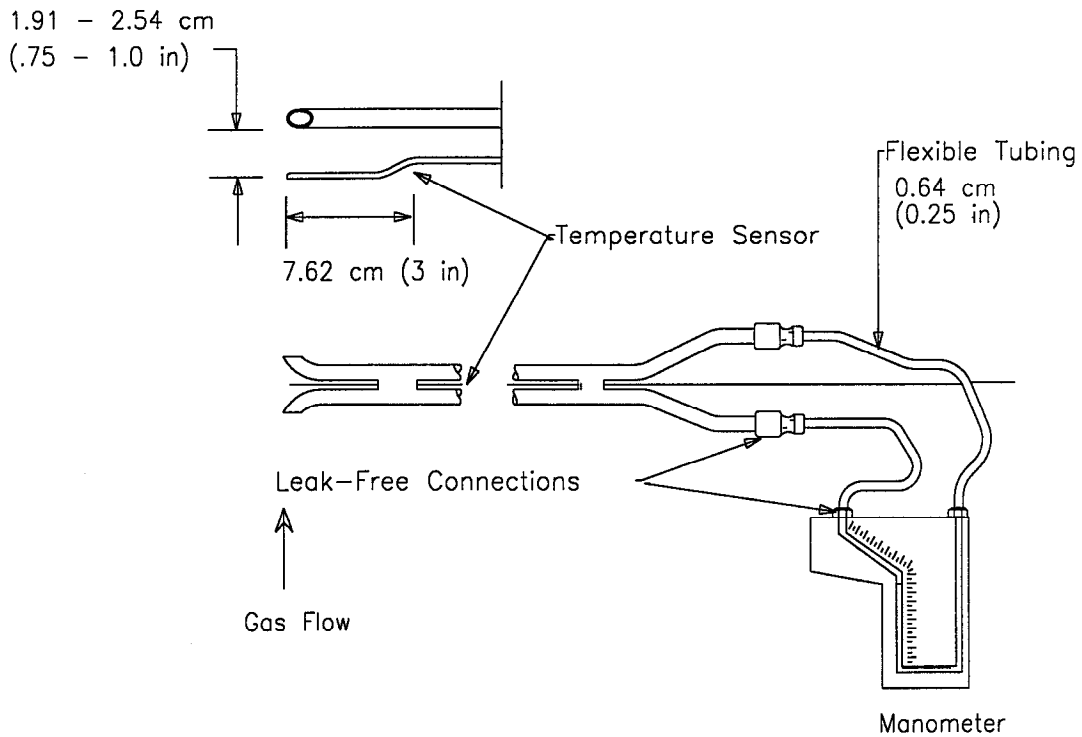


| Point | % of diameter | Inches from wall | Inches from port edge |
|-------|---------------|------------------|-----------------------|
| 1 | 3.2 | 6.9 | 13.9 |
| 2 | 10.5 | 22.7 | 29.7 |
| 3 | 19.4 | 41.9 | 48.9 |
| 4 | 32.3 | 69.8 | 76.8 |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |

Pre-cyclonic flow check conducted? No Reason: Conducted Previously

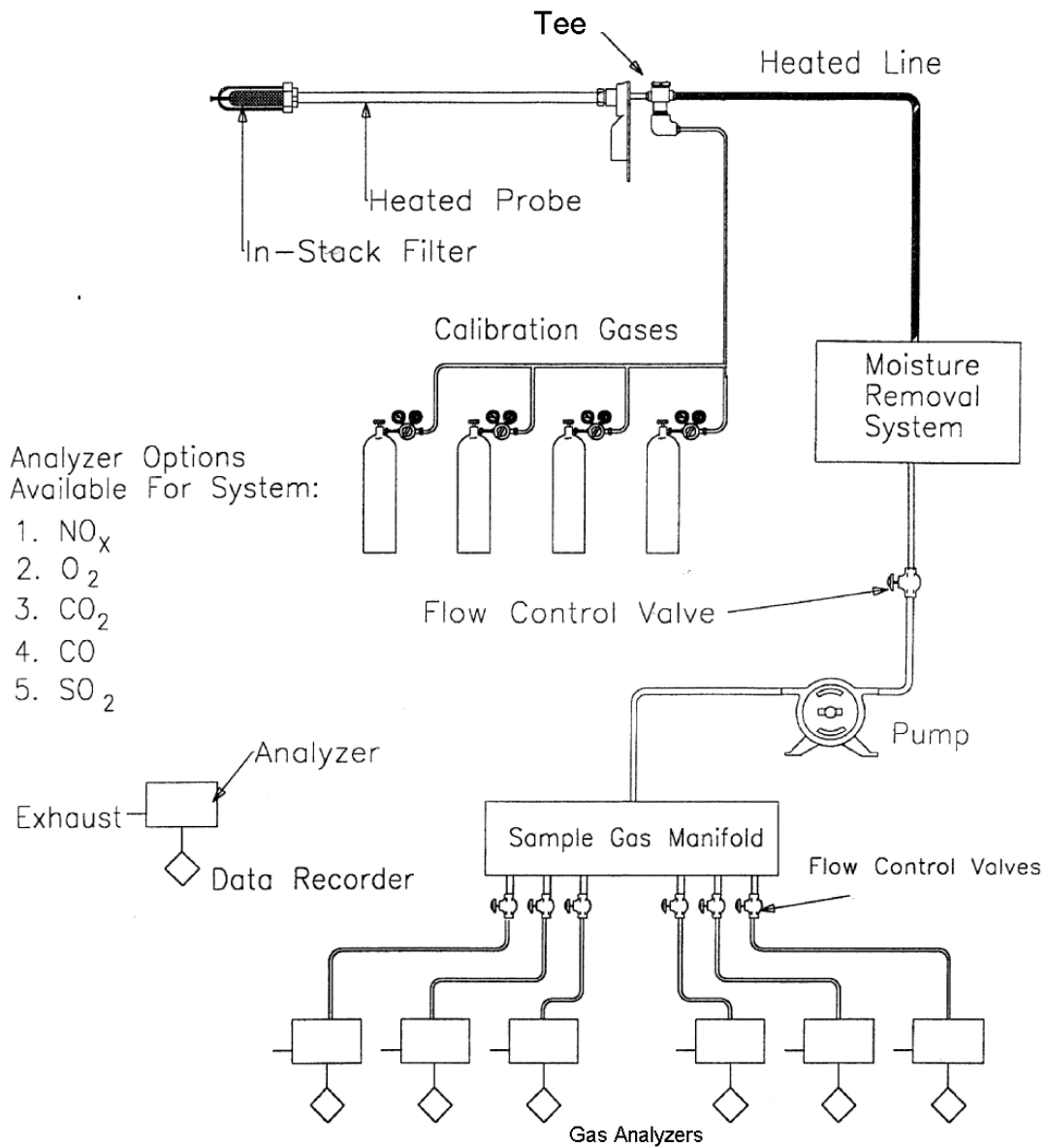
Determination of Stack Gas Velocity and Volumetric Flow Rate

USEPA Promulgated Test Method 2



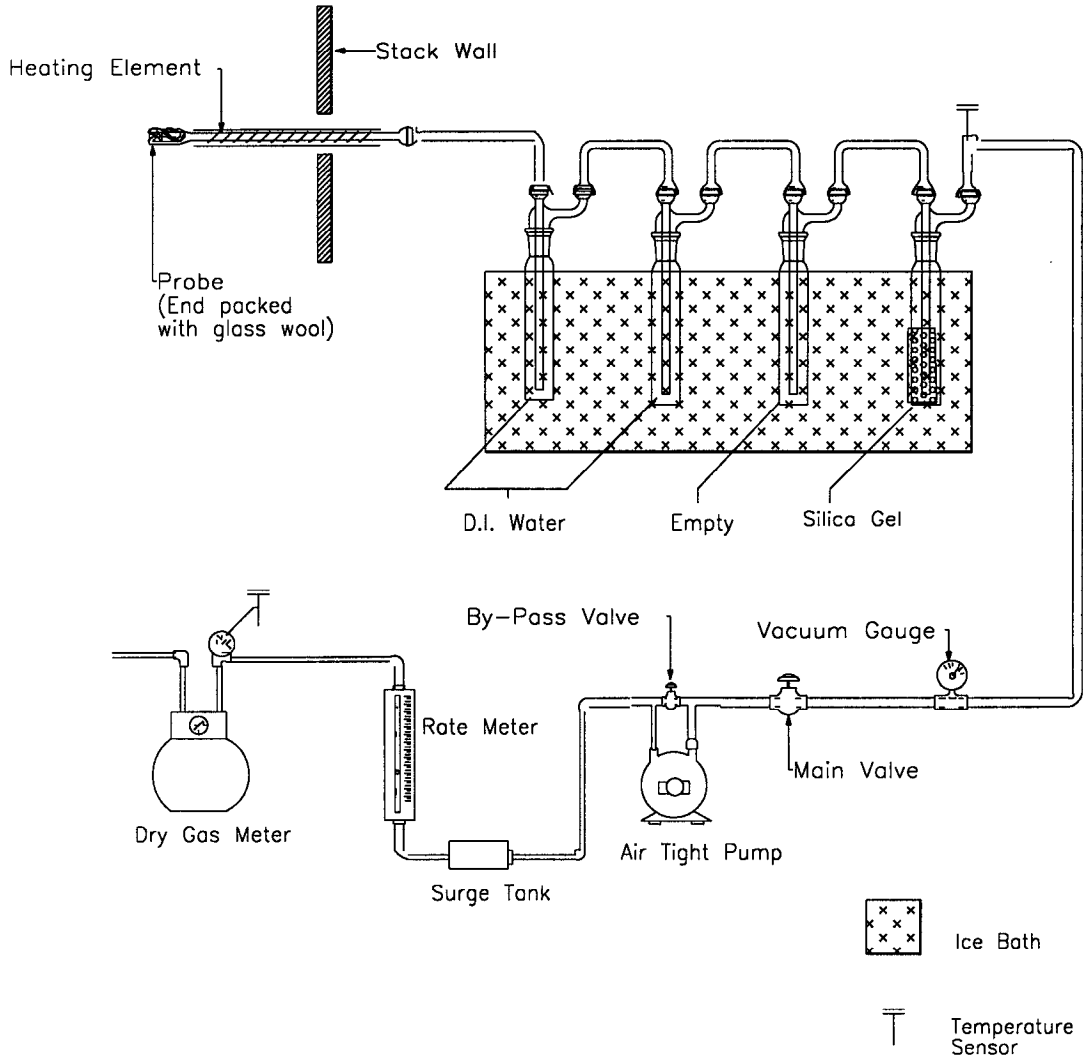
Determination of Multiple Gaseous Pollutants Using an Extractive Sampling Train

USEPA Promulgated Methods 3A, 6C and 10



Determination of Moisture Content in Stack Gases

USEPA Promulgated Method 4





Example Calculations - Method 2 Volumetric Flow

Company: Primary Energy
Unit ID: HRCC
Plant: Cokenergy Facility
Sample Location: Stack 201

Project Number: 305091
Test Date: September 12, 2018
Run #: 1
Operating Level: High

Note: In order to duplicate these examples, results must not be rounded.

Effluent Gas Pressure

$$P_s = P_{bar} + (P_g/13.6)$$

Where:

P_s = Flue gas pressure ("Hg)
 P_{bar} = Ambient barometric pressure at sample elevation ("Hg)
 P_g = Flue gas gauge pressure ("H₂O)

P_{bar} = 29.26 "Hg P_g = -1 "H₂O

P_s = 29.19 "Hg

Average Stack Temperature

$$T_s = \frac{\sum_{i=1}^n T_{si}}{n}$$

Where:

T_s = Average effluent gas temperature (°F)
 T_{si} = Effluent gas temperature at point i (°F)
 n = Total number of traverse points

T_s = 287 °F

Actual Meter Volume

$$V_m = V_f - V_i$$

Where:

V_i = Initial meter sample volume (cubic feet)
 V_f = Final meter sample volume (cubic feet)
 V_m = Sample volume collected at actual conditions (ft³, dry basis)

V_f = 301.456 cf V_i = 279.000 cf

V_m = 22.456 cubic feet

Example Calculations - Method 2 Volumetric Flow

| | | | |
|------------------|---------------------------|------------------|---------------------------|
| Company: | <u>Primary Energy</u> | Project Number: | <u>305091</u> |
| Unit ID: | <u>HRCC</u> | Test Date: | <u>September 12, 2018</u> |
| Plant: | <u>Cokenergy Facility</u> | Run #: | <u>1</u> |
| Sample Location: | <u>Stack 201</u> | Operating Level: | <u>High</u> |

Note: In order to duplicate these examples, results must not be rounded.

Standard Meter Volume

$$V_{m(std)} = T_{std}/29.92 \times Y \times V_m \times (P_{bar} + \Delta H /13.6)/(T_m + 460)$$

Where:

- $V_{m(std)}$ = Sample volume collected corrected to 29.92"Hg and T_{std} (scf, dry basis)
- Y = Dry test meter calibration coefficient (dimensionless)
- V_m = Sample volume collected at actual conditions (ft³, dry basis)
- T_m = Average dry test meter temperature (°F)
- ΔH = Pressure drop across calibrated orifice ("H₂O)
- T_{std} = Standard Temperature (°R)

| | |
|--|------------------------------|
| $V_m =$ <u>22.456</u> cf | $P_{bar} =$ <u>29.26</u> "Hg |
| $\Delta H =$ <u>2.00</u> "H ₂ O | $T_m =$ <u>70.9</u> °F |
| Y = <u>0.997</u> dimensionless | $T_{std} =$ <u>528</u> °R |

$$V_{m(std)} = \underline{21.885} \text{ dscf}$$

Volume of Water Vapor Condensed

$$V_{w(std)} = [(0.04707 \times \text{net ml H}_2\text{O}) + (0.04715 \times \text{net grams H}_2\text{O})] \times (T_{std} / 528)$$

Where:

$V_{w(std)}$ = Sample volume collected corrected to 29.92 in. Hg and 528(°R) (ft³, dry basis)

net grams H₂O = Final moisture weight - initial moisture weight

net grams H₂O = 3182.6 - 3108.3

$$V_{w(std)} = \underline{3.503} \text{ cf}$$

Moisture Content From Method 4 or Alt-008

$$B_{ws} = \frac{V_{w(std)}}{V_{w(std)} + V_{m(std)}}$$

Where:

B_{ws} = Fractional moisture content (dimensionless)

| | |
|--------------------------------|-----------------------------------|
| $V_{w(std)} =$ <u>3.503</u> cf | $V_{m(std)} =$ <u>21.885</u> dscf |
|--------------------------------|-----------------------------------|

$$B_{ws} = \underline{0.138}$$

Example Calculations - Method 2 Volumetric Flow

| | | | |
|------------------|---------------------------|------------------|---------------------------|
| Company: | <u>Primary Energy</u> | Project Number: | <u>305091</u> |
| Unit ID: | <u>HRCC</u> | Test Date: | <u>September 12, 2018</u> |
| Plant: | <u>Cokenergy Facility</u> | Run #: | <u>1</u> |
| Sample Location: | <u>Stack 201</u> | Operating Level: | <u>High</u> |

Note: In order to duplicate these examples, results must not be rounded.

Dry Molecular Weight

$$M_d = 0.44 \times (\%CO_2) + 0.32 \times (\%O_2) + 0.28 \times (\%N_2)$$

Where:

- M_d = Effluent gas molecular weight (lb/lb-mole, dry basis)
- $\%CO_2$ = Effluent gas Carbon Dioxide Content (% volume, dry basis)
- $\%O_2$ = Effluent gas Oxygen Content (% volume, dry basis)
- $\%N_2$ = Effluent Balance Gas Content (% volume, dry basis)
- 0.32 = Molecular weight of O2 divided by 100
- 0.44 = Molecular weight of CO2 divided by 100
- 0.28 = Molecular weight of Nitrogen divided by 100

$$\%CO_2 = \underline{5.2} \qquad \%O_2 = \underline{12.6} \qquad \%N_2 = \underline{82.2}$$

$$M_d = \underline{29.34} \text{ lb/lb-mole} \qquad \text{From Method 3A, Instrumental}$$

Wet Molecular Weight

$$M_s = M_d \times (1 - B_{ws}) + (18.0 \times B_{ws})$$

Where:

- M_s = Effluent gas molecular weight (lb/lb-mole, wet basis)
- B_{ws} = Effluent gas fractional moisture content (dimensionless)

$$M_d = \underline{29.34} \text{ lb/lb-mole} \qquad B_{ws} = \underline{0.138} \text{ From Method 4}$$

$$M_s = \underline{27.77} \text{ lb/lb-mole}$$

Average Square Root of Velocity Head - applicable to Method 2 only

$$avg\sqrt{\Delta P} = \frac{\sum_{i=1}^n \sqrt{\Delta P_i}}{n}$$

Where:

- $\sqrt{\Delta P_i}$ = square root of ΔP at traverse point i
- $avg\sqrt{\Delta P}$ = Average of the square roots of ΔP 's at all traverse points

$$avg\sqrt{\Delta P} = \underline{1.0275}$$



Example Calculations - Method 2 Volumetric Flow

| | | | |
|------------------|---------------------------|------------------|---------------------------|
| Company: | <u>Primary Energy</u> | Project Number: | <u>305091</u> |
| Unit ID: | <u>HRCC</u> | Test Date: | <u>September 12, 2018</u> |
| Plant: | <u>Cokenergy Facility</u> | Run #: | <u>1</u> |
| Sample Location: | <u>Stack 201</u> | Operating Level: | <u>High</u> |

Note: In order to duplicate these examples, results must not be rounded.

Average Duct Velocity - applicable to Method 2 only

$$V_s = 85.49 \times C_p \times \text{avg}\sqrt{\Delta P} \times ((T_s + 460) / (P_s \times M_s))^{1/2}$$

Where:

V_s = Average velocity of effluent gas (ft/sec)

C_p = Pitot calibration coefficient (dimensionless)

$\text{avg}\sqrt{\Delta P}$ = Average of the square roots of ΔP 's at all traverse points

T_s = Average effluent gas temperature ($^{\circ}\text{F}$)

$$C_p = \frac{0.840}{1} \\ P_s = \frac{29.19}{1} \text{ "Hg} \\ \text{avg}\sqrt{\Delta P} = \frac{1.0275}{1}$$

$$T_s = \frac{287}{1} \text{ }^{\circ}\text{F} \\ M_s = \frac{27.77}{1} \text{ lb/lb-mole}$$

$$V_s = \underline{70.81} \text{ ft/sec}$$

Volumetric Flow Rate (Actual Basis)

Applicable when Method 2 is used alone:

$$Q_{acfm} = V_s \times A \times 60 \text{ sec/min}$$

Where:

Q = Effluent gas volumetric flow rate at actual conditions (acfm)

A = Cross-sectional area of the stack/duct at the test location (ft^2)

$$V_s = \underline{70.81} \text{ ft/sec}$$

$$A = \underline{254.469} \text{ ft}^2$$

$$Q = \underline{1,081,203} \text{ acfm}$$



Example Calculations - Method 2 Volumetric Flow

Company: Primary Energy
Unit ID: HRCC
Plant: Cokenergy Facility
Sample Location: Stack 201

Project Number: 305091
Test Date: September 12, 2018
Run #: 1
Operating Level: High

Note: In order to duplicate these examples, results must not be rounded.

Volumetric Flow Rate (Standard Wet Basis)

Standard cubic feet per minute (Wet):

$$Q_{std} = Q \times (T_{std}/29.92) \times (P_s/(T_s + 460))$$

Where:

Q_{std} = Effluent gas volumetric flow rate corrected to 29.92"Hg and 528°R (scfm)

$Q =$ 1,081,203 scfm

$P_s =$ 29.19 "Hg

T_s (avg) = 287 °F

$T_{std} =$ 528 °R

$Q_{std} =$ 745,862 scfm

Standard cubic feet per hour (Wet):

$$Q_{sw} = Q_{std} \times 60 \text{ min/hr}$$

$Q_{sw} =$ 44,751,720 scfh

Volumetric Flow Rate (Standard Dry Basis)

Standard cubic feet per minute (Dry):

$$Q_{dscfm} = Q_{std} \times (1 - B_{ws})$$

$B_{ws} =$ 0.138 dimensionless

$Q_{dscfm} =$ 642,941 dscfm

Standard cubic feet per hour (Dry):

$$Q_{sd} = Q_{dscfm} \times 60 \text{ min/hr}$$

$Q_{sd} =$ 38,576,474 dscfh



Example Calculations - Effluent Gas Concentration Determination

| | | | |
|----------------------|-----------------------|------------|---------------------------|
| Project Number: | <u>305091</u> | Test Date: | <u>September 12, 2018</u> |
| Customer: | <u>Primary Energy</u> | Facility: | <u>Cokenergy Facility</u> |
| Unit Identification: | <u>HRCC</u> | Run #: | <u>1</u> |
| Sample Location: | <u>Stack 201</u> | | |

$$C_{\text{gas}} = (C - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

Where:

C_{gas} = Effluent gas concentration (ppm or %vol)

C = Average gas concentration indicated by analyzer (ppm or %vol)

C_0 = Average of pre- and post-test system bias checks using low range gas (ppm or % vol)

C_{m} = Average of pre- and post-test system bias checks using upscale gas (ppm or % vol)

C_{ma} = Actual concentration of upscale gas (ppm or % vol)

| | | | | |
|-----------------------|------------------|------------|-------------------|-----------|
| SO₂ | $C =$ | 152.39 ppm | $C_0 =$ | 2.90 ppm |
| | $C_{\text{m}} =$ | 196.95 ppm | $C_{\text{ma}} =$ | 201.8 ppm |

$C_{\text{SO}_2} = 155.5 \text{ ppm}$

| | | | | |
|-----------------------|------------------|-----------|-------------------|------------|
| CO₂ | $C =$ | 5.16 %vol | $C_0 =$ | 0.05 %vol |
| | $C_{\text{m}} =$ | 8.77 %vol | $C_{\text{ma}} =$ | 8.798 %vol |

$C_{\text{CO}_2} = 5.2 \text{ %vol}$

| | | | | |
|----------------------|------------------|------------|-------------------|------------|
| O₂ | $C =$ | 12.58 %vol | $C_0 =$ | 0.05 %vol |
| | $C_{\text{m}} =$ | 9.98 %vol | $C_{\text{ma}} =$ | 9.976 %vol |

$C_{\text{O}_2} = 12.6 \text{ %vol}$

Note: Interim results are not rounded.



Example Calculations - Pollutant Emission Rate, Volumetric Flow Rate-Based

| | | | |
|----------------------|-----------------------|------------|---------------------------|
| Project Number: | <u>305091</u> | Test Date: | <u>September 12, 2018</u> |
| Customer: | <u>Primary Energy</u> | Facility: | <u>Cokenergy Facility</u> |
| Unit Identification: | <u>HRCC</u> | Run #: | <u>1</u> |

$$ER = C_{gas} \times C_f \times Flow \times 60$$

Where:

ER = Pollutant emission rate (lb/hr)

C_{gas} = Pollutant concentration (ppm, wet or dry basis, but the same as flow)

MW = Pollutant molecular weight (gr/gr-mole)

Flow = Volumetric flow rate (cubic feet per minute wet or dry, but the same as C_{gas})

C_f = Conversion factor (ppm to lb/scf)

1.660E-07 = Conversion constant for SO₂. From Table 19-1 of Method 19, 40CFR, Appendix A

For SO₂

$$ER = C_{gas} \times 1.660E-07 \times Flow \times 60$$

$C_{gas} = 155.5$ ppmvd
Flow = 642,941 DSCFM

$$ER_{SO_2} = 995.53 \text{ lb/hr}$$

Note: Interim results are not rounded.



Example Calculations - Relative Accuracy (RA) and Bias

| | | | |
|----------------------|-----------------------|------------|---------------------------|
| Project Number: | <u>305091</u> | Test Date: | <u>September 12, 2018</u> |
| Customer: | <u>Primary Energy</u> | Facility: | <u>Cokenergy Facility</u> |
| Unit Identification: | <u>HRCC</u> | | |

Mean Difference:

$$\bar{d} = \frac{1}{n} \sum_{i=1}^n d_i$$

Where:

d_i = Difference between RM and CEMS values for run "i"

n = Number of runs used to calculate RA

Standard Deviation:

$$Sd = \left[\frac{\sum_{i=1}^n d_i^2 - \frac{\left[\sum_{i=1}^n d_i \right]^2}{n}}{n - 1} \right]^{1/2}$$

Confidence Coefficient:

$$CC = t_{0.025} \frac{Sd}{\sqrt{n}}$$

Where:

$t_{0.025}$ = T values as presented in 40CFR60 or 40CFR75.
For 40CFR60, use $t_{0.975}$, which are the same T values.

Relative Accuracy based on RM:

$$RA = \frac{|\bar{d}| + |CC|}{RM \text{ avg}} \times 100$$

Where:

RM avg = Average RM value for runs used to calculate RA

Relative Accuracy based on Applicable Standard - for Part 60 Applications Only:

$$RA = \frac{|\bar{d}| + |CC|}{App \text{ Std}} \times 100$$



Example Calculations - Moisture (Method 4)

| | | | |
|------------------|---------------------------|------------------|---------------------------|
| Company: | <u>Primary Energy</u> | Project Number: | <u>305091</u> |
| Plant: | <u>Cokenergy Facility</u> | Test Date: | <u>September 12, 2018</u> |
| Unit ID: | <u>HRCC</u> | Run #: | <u>1</u> |
| Sample Location: | <u>Stack 201</u> | Operating Level: | <u>High</u> |

Effluent Gas Pressure

$$P_s = P_{bar} + (P_g / 13.6)$$

Where:

P_s = Flue gas pressure ("Hg)

P_{bar} = Ambient barometric pressure at sample elevation ("Hg)

P_g = Flue gas gauge pressure ("H₂O)

$$P_{bar} = \underline{29.26} \text{ "Hg}$$

$$P_g = \underline{-1.00} \text{ "H}_2\text{O}$$

$$P_s = \underline{29.19} \text{ "Hg}$$

Actual Meter Volume

$$V_m = V_f - V_i$$

Where:

V_i = Initial meter sample volume (Cubic Feet or Liters)

V_f = Final meter sample volume (Cubic Feet or Liters)

V_m = Sample volume collected at actual conditions (dcf)

$$V_f = \underline{301.456} \text{ cf}$$

$$V_i = \underline{279.000} \text{ cf}$$

$$V_m = \underline{22.456} \text{ dcf}$$

Sample Volume at Standard Conditions

$$V_{m(std)} = (T_{std} / 29.92) \times Y \times V_m \times (P_{bar} + P_m / 13.6) / (T_m + 460)$$

Where:

$V_{m(std)}$ = Sample volume collected corrected to 29.92 "Hg and 528 °R (dscf)

Y = Dry test meter calibration coefficient (dimensionless)

T_m = Average dry test meter temperature (°F)

P_m = Average dry test meter pressure ("H₂O)

T_{std} = Standard temperature 528 °R

$$V_m = \underline{22.456} \text{ dcf}$$

$$P_{bar} = \underline{29.26} \text{ "Hg}$$

$$P_m = \underline{2.00} \text{ "H}_2\text{O}$$

$$T_m = \underline{70.9} \text{ °F}$$

$$Y = \underline{0.997}$$

$$T_{std} = \underline{528.0} \text{ °R}$$

$$V_{m(std)} = \underline{21.884} \text{ dscf}$$



Example Calculations - Moisture (Method 4)

| | | | |
|------------------|---------------------------|------------------|---------------------------|
| Company: | <u>Primary Energy</u> | Project Number: | <u>305091</u> |
| Plant: | <u>Cokenergy Facility</u> | Test Date: | <u>September 12, 2018</u> |
| Unit ID: | <u>HRCC</u> | Run #: | <u>1</u> |
| Sample Location: | <u>Stack 201</u> | Operating Level: | <u>High</u> |

Volume of Water Vapor Condensed at Standard Conditions

$$V_{wc(std)} = 0.04715 \times (T_{std} / 528) \times M_{H_2O}$$

Where:

$V_{wc(std)}$ = Volume of water vapor collected corrected to 29.92 "Hg and 528 °R (scf)

M_{H_2O} = Net weight gain of impingers (grams)

$$M_{H_2O} = \underline{74.3} \text{ grams}$$

$$V_{wc(std)} = \underline{3.503} \text{ scf}$$

Moisture Content

$$B_{ws} = \frac{V_{wc(std)}}{V_{wc(std)} + V_{m(std)}}$$

Where:

B_{ws} = Fractional moisture content (dimensionless)

$$V_{wc(std)} = \underline{3.503} \text{ scf}$$

$$V_{m(std)} = \underline{21.884} \text{ dscf}$$

$$B_{ws} = \underline{0.138}$$

Dry Molecular Weight

$$M_d = 0.44 \times (\%CO_2) + 0.32 \times (\%O_2) + 0.28 \times (\%N_2)$$

Where:

M_d = Effluent gas molecular weight (lb/lb-mole, dry basis)

$\%CO_2$ = Effluent gas Carbon Dioxide Content (% volume, dry basis)

$\%O_2$ = Effluent gas Oxygen Content (% volume, dry basis)

$\%N_2$ = Effluent gas Nitrogen Content (% volume, dry basis)

0.32 = Molecular weight of O_2 , divided by 100

0.44 = Molecular weight of CO_2 , divided by 100

0.28 = Molecular weight of N_2 , divided by 100

$$\%CO_2 = \underline{5.2}$$

$$\%O_2 = \underline{12.6}$$

$$\%N_2 = \underline{82.2}$$

$$M_d = \underline{29.34} \text{ lb/lb-mole}$$

Wet Molecular Weight

$$M_s = M_d \times (1 - B_{ws}) + (18.0 \times B_{ws})$$

Where:

M_s = Effluent gas molecular weight (lb/lb-mole, wet basis)

$$M_d = \underline{29.34} \text{ lb/lb-mole}$$

$$B_{ws} = \underline{0.138}$$

$$M_s = \underline{27.77} \text{ lb/lb-mole}$$



Instrumental Reference Method Field Data

| | |
|--|-------------------------------------|
| Project Number: <u>305091</u> | Start Date: <u>9/12/2018</u> |
| Customer: <u>Primary Energy</u> | End Date: <u>9/12/2018</u> |
| Unit Identification: <u>HRCC</u> | Facility: <u>Cokenergy Facility</u> |
| Sample Location: <u>Stack 201</u> | Recorded by: <u>Gavin Lewis</u> |
| Load Level/Condition: <u>> 50% load</u> | Fc Factor: <u>-</u> |
| | Fd Factor: <u>-</u> |

| Test Parameter | | | | NO _x | SO ₂ | CO | CO ₂ | O ₂ | Volumetric Flow Rate | Moisture Fraction |
|------------------------------|------------|--------------|-------------|------------------------------------|-----------------|----|-----------------|----------------|----------------------|-------------------|
| Calibration Span, CS (Day 1) | | | | - | 452.6 | - | 17.86 | 22.01 | | |
| Calibration Span, CS (Day 2) | | | | - | - | - | - | - | | |
| Run No. | Start Date | First Minute | Last Minute | Run Average Raw Analyzer Responses | | | | | DSCFM | Bws |
| 1 | 9/12/18 | 7:15 | 7:35 | - | 152.39 | - | 5.16 | 12.58 | 642941 | - |
| 2 | 9/12/18 | 8:00 | 8:20 | - | 148.93 | - | 5.11 | 12.70 | 652324 | - |
| 3 | 9/12/18 | 8:40 | 9:00 | - | 152.98 | - | 5.06 | 12.80 | 631745 | - |
| 4 | 9/12/18 | 9:20 | 9:40 | - | 143.08 | - | 4.96 | 12.99 | 623188 | - |
| 5 | 9/12/18 | 10:00 | 10:20 | - | 137.82 | - | 4.98 | 12.98 | 625367 | - |
| 6 | 9/12/18 | 10:45 | 11:05 | - | 130.89 | - | 4.94 | 13.06 | 633954 | - |
| 7 | 9/12/18 | 11:25 | 11:45 | - | 132.54 | - | 4.87 | 13.19 | 629515 | - |
| 8 | 9/12/18 | 12:05 | 12:25 | - | 133.23 | - | 4.76 | 13.38 | 636072 | - |
| 9 | 9/12/18 | 12:45 | 13:05 | - | 126.67 | - | 4.70 | 13.48 | 632043 | - |
| 10 | 9/12/18 | 13:25 | 13:45 | - | 121.24 | - | 4.73 | 13.47 | 619433 | - |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Run 1

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|---------------|-------------|--------------|
| 9/12/2018 7:15 | 153.39 | 5.19 | 12.55 |
| 9/12/2018 7:16 | 153.63 | 5.16 | 12.59 |
| 9/12/2018 7:17 | 154.13 | 5.18 | 12.56 |
| 9/12/2018 7:18 | 153.79 | 5.18 | 12.56 |
| 9/12/2018 7:19 | 155.88 | 5.15 | 12.60 |
| 9/12/2018 7:20 | 155.38 | 5.17 | 12.57 |
| 9/12/2018 7:21 | 149.20 | 5.17 | 12.56 |
| 9/12/2018 7:22 | 150.62 | 5.15 | 12.60 |
| 9/12/2018 7:23 | 151.50 | 5.18 | 12.56 |
| 9/12/2018 7:24 | 150.63 | 5.16 | 12.58 |
| 9/12/2018 7:25 | 153.38 | 5.15 | 12.60 |
| 9/12/2018 7:26 | 151.51 | 5.16 | 12.58 |
| 9/12/2018 7:27 | 151.44 | 5.18 | 12.56 |
| 9/12/2018 7:28 | 151.78 | 5.15 | 12.60 |
| 9/12/2018 7:29 | 152.94 | 5.16 | 12.58 |
| 9/12/2018 7:30 | 151.12 | 5.18 | 12.56 |
| 9/12/2018 7:31 | 152.55 | 5.15 | 12.59 |
| 9/12/2018 7:32 | 152.24 | 5.16 | 12.60 |
| 9/12/2018 7:33 | 152.97 | 5.16 | 12.58 |
| 9/12/2018 7:34 | 151.03 | 5.16 | 12.59 |
| 9/12/2018 7:35 | 151.00 | 5.15 | 12.59 |
| Average | 152.39 | 5.16 | 12.58 |

Run 2

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|---------------|-------------|--------------|
| 9/12/2018 8:00 | 146.48 | 5.11 | 12.71 |
| 9/12/2018 8:01 | 148.38 | 5.13 | 12.68 |
| 9/12/2018 8:02 | 147.88 | 5.13 | 12.67 |
| 9/12/2018 8:03 | 149.52 | 5.10 | 12.70 |
| 9/12/2018 8:04 | 148.57 | 5.12 | 12.68 |
| 9/12/2018 8:05 | 148.60 | 5.10 | 12.70 |
| 9/12/2018 8:06 | 147.16 | 5.12 | 12.67 |
| 9/12/2018 8:07 | 149.76 | 5.10 | 12.70 |
| 9/12/2018 8:08 | 148.26 | 5.12 | 12.67 |
| 9/12/2018 8:09 | 148.04 | 5.09 | 12.72 |
| 9/12/2018 8:10 | 147.37 | 5.12 | 12.67 |
| 9/12/2018 8:11 | 147.99 | 5.08 | 12.72 |
| 9/12/2018 8:12 | 148.38 | 5.13 | 12.65 |
| 9/12/2018 8:13 | 149.53 | 5.09 | 12.71 |
| 9/12/2018 8:14 | 150.11 | 5.10 | 12.69 |
| 9/12/2018 8:15 | 148.65 | 5.10 | 12.71 |
| 9/12/2018 8:16 | 149.03 | 5.09 | 12.72 |
| 9/12/2018 8:17 | 150.20 | 5.10 | 12.71 |
| 9/12/2018 8:18 | 149.89 | 5.11 | 12.70 |
| 9/12/2018 8:19 | 150.94 | 5.10 | 12.71 |
| 9/12/2018 8:20 | 152.77 | 5.09 | 12.72 |
| Average | 148.93 | 5.11 | 12.70 |

Run 3

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|---------------|-------------|--------------|
| 9/12/2018 8:40 | 149.49 | 5.08 | 12.75 |
| 9/12/2018 8:41 | 151.45 | 5.06 | 12.79 |
| 9/12/2018 8:42 | 149.95 | 5.08 | 12.75 |
| 9/12/2018 8:43 | 151.99 | 5.05 | 12.79 |
| 9/12/2018 8:44 | 151.41 | 5.09 | 12.75 |
| 9/12/2018 8:45 | 152.70 | 5.06 | 12.79 |
| 9/12/2018 8:46 | 154.51 | 5.06 | 12.79 |
| 9/12/2018 8:47 | 153.76 | 5.08 | 12.77 |
| 9/12/2018 8:48 | 153.97 | 5.07 | 12.79 |
| 9/12/2018 8:49 | 156.88 | 5.06 | 12.80 |
| 9/12/2018 8:50 | 154.38 | 5.08 | 12.78 |
| 9/12/2018 8:51 | 153.46 | 5.04 | 12.83 |
| 9/12/2018 8:52 | 152.20 | 5.07 | 12.79 |
| 9/12/2018 8:53 | 151.19 | 5.06 | 12.81 |
| 9/12/2018 8:54 | 153.90 | 5.05 | 12.81 |
| 9/12/2018 8:55 | 152.99 | 5.06 | 12.79 |
| 9/12/2018 8:56 | 155.48 | 5.04 | 12.83 |
| 9/12/2018 8:57 | 153.33 | 5.06 | 12.79 |
| 9/12/2018 8:58 | 153.66 | 5.04 | 12.87 |
| 9/12/2018 8:59 | 153.58 | 5.03 | 12.87 |
| 9/12/2018 9:00 | 152.39 | 5.04 | 12.83 |
| Average | 152.98 | 5.06 | 12.80 |

Run 4

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|---------------|-------------|--------------|
| 9/12/2018 9:20 | 136.04 | 4.90 | 13.09 |
| 9/12/2018 9:21 | 135.92 | 4.91 | 13.08 |
| 9/12/2018 9:22 | 134.26 | 4.91 | 13.08 |
| 9/12/2018 9:23 | 137.31 | 4.91 | 13.09 |
| 9/12/2018 9:24 | 137.41 | 4.91 | 13.09 |
| 9/12/2018 9:25 | 138.78 | 4.94 | 13.03 |
| 9/12/2018 9:26 | 142.21 | 4.96 | 12.99 |
| 9/12/2018 9:27 | 144.28 | 4.98 | 12.98 |
| 9/12/2018 9:28 | 145.34 | 4.99 | 12.94 |
| 9/12/2018 9:29 | 146.28 | 4.97 | 12.97 |
| 9/12/2018 9:30 | 148.57 | 4.97 | 12.95 |
| 9/12/2018 9:31 | 146.49 | 4.97 | 12.96 |
| 9/12/2018 9:32 | 146.75 | 4.97 | 12.97 |
| 9/12/2018 9:33 | 146.00 | 4.98 | 12.95 |
| 9/12/2018 9:34 | 146.86 | 4.98 | 12.96 |
| 9/12/2018 9:35 | 146.71 | 4.99 | 12.94 |
| 9/12/2018 9:36 | 144.99 | 4.98 | 12.96 |
| 9/12/2018 9:37 | 145.17 | 5.00 | 12.93 |
| 9/12/2018 9:38 | 143.97 | 4.98 | 12.96 |
| 9/12/2018 9:39 | 146.38 | 4.98 | 12.95 |
| 9/12/2018 9:40 | 144.94 | 4.99 | 12.94 |
| Average | 143.08 | 4.96 | 12.99 |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Run 5

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|---------------|-------------|--------------|
| 9/12/2018 10:00 | 136.10 | 5.00 | 12.94 |
| 9/12/2018 10:01 | 136.51 | 5.00 | 12.95 |
| 9/12/2018 10:02 | 137.08 | 4.99 | 12.96 |
| 9/12/2018 10:03 | 137.12 | 4.98 | 12.97 |
| 9/12/2018 10:04 | 136.65 | 5.00 | 12.95 |
| 9/12/2018 10:05 | 137.52 | 4.98 | 12.98 |
| 9/12/2018 10:06 | 139.17 | 4.98 | 12.97 |
| 9/12/2018 10:07 | 138.78 | 4.98 | 12.97 |
| 9/12/2018 10:08 | 139.75 | 4.98 | 12.98 |
| 9/12/2018 10:09 | 139.79 | 4.99 | 12.96 |
| 9/12/2018 10:10 | 139.86 | 4.97 | 12.99 |
| 9/12/2018 10:11 | 141.38 | 4.98 | 12.98 |
| 9/12/2018 10:12 | 140.09 | 4.98 | 12.99 |
| 9/12/2018 10:13 | 137.45 | 4.95 | 13.02 |
| 9/12/2018 10:14 | 136.04 | 4.98 | 12.99 |
| 9/12/2018 10:15 | 137.38 | 4.96 | 12.99 |
| 9/12/2018 10:16 | 136.46 | 4.96 | 13.00 |
| 9/12/2018 10:17 | 137.79 | 4.97 | 13.00 |
| 9/12/2018 10:18 | 138.05 | 4.97 | 12.98 |
| 9/12/2018 10:19 | 135.44 | 4.96 | 13.00 |
| 9/12/2018 10:20 | 135.88 | 4.95 | 13.02 |
| Average | 137.82 | 4.98 | 12.98 |

Run 6

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|---------------|-------------|--------------|
| 9/12/2018 10:45 | 130.06 | 4.94 | 13.06 |
| 9/12/2018 10:46 | 132.01 | 4.96 | 13.03 |
| 9/12/2018 10:47 | 129.32 | 4.96 | 13.03 |
| 9/12/2018 10:48 | 132.09 | 4.94 | 13.06 |
| 9/12/2018 10:49 | 129.68 | 4.95 | 13.04 |
| 9/12/2018 10:50 | 131.17 | 4.93 | 13.06 |
| 9/12/2018 10:51 | 131.86 | 4.94 | 13.05 |
| 9/12/2018 10:52 | 131.84 | 4.94 | 13.06 |
| 9/12/2018 10:54 | 131.26 | 4.95 | 13.03 |
| 9/12/2018 10:55 | 131.13 | 4.93 | 13.06 |
| 9/12/2018 10:56 | 132.26 | 4.94 | 13.06 |
| 9/12/2018 10:57 | 131.19 | 4.94 | 13.05 |
| 9/12/2018 10:58 | 131.11 | 4.92 | 13.07 |
| 9/12/2018 10:59 | 131.57 | 4.93 | 13.06 |
| 9/12/2018 11:00 | 130.95 | 4.94 | 13.06 |
| 9/12/2018 11:01 | 129.33 | 4.94 | 13.05 |
| 9/12/2018 11:02 | 130.34 | 4.93 | 13.07 |
| 9/12/2018 11:03 | 129.51 | 4.94 | 13.05 |
| 9/12/2018 11:04 | 131.29 | 4.92 | 13.09 |
| 9/12/2018 11:05 | 130.60 | 4.93 | 13.06 |
| 9/12/2018 11:06 | 130.07 | 4.93 | 13.08 |
| Average | 130.89 | 4.94 | 13.06 |

Run 7

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|---------------|-------------|--------------|
| 9/12/2018 11:25 | 127.25 | 4.89 | 13.14 |
| 9/12/2018 11:26 | 129.47 | 4.88 | 13.15 |
| 9/12/2018 11:27 | 129.91 | 4.89 | 13.14 |
| 9/12/2018 11:28 | 129.33 | 4.86 | 13.18 |
| 9/12/2018 11:29 | 132.13 | 4.88 | 13.16 |
| 9/12/2018 11:30 | 130.09 | 4.87 | 13.17 |
| 9/12/2018 11:31 | 130.45 | 4.86 | 13.20 |
| 9/12/2018 11:32 | 132.17 | 4.87 | 13.18 |
| 9/12/2018 11:33 | 131.10 | 4.87 | 13.18 |
| 9/12/2018 11:34 | 132.28 | 4.85 | 13.21 |
| 9/12/2018 11:35 | 132.25 | 4.88 | 13.17 |
| 9/12/2018 11:36 | 132.43 | 4.89 | 13.16 |
| 9/12/2018 11:37 | 133.48 | 4.86 | 13.20 |
| 9/12/2018 11:38 | 135.23 | 4.87 | 13.19 |
| 9/12/2018 11:39 | 133.28 | 4.86 | 13.20 |
| 9/12/2018 11:40 | 133.55 | 4.86 | 13.20 |
| 9/12/2018 11:41 | 134.86 | 4.84 | 13.23 |
| 9/12/2018 11:42 | 134.68 | 4.86 | 13.20 |
| 9/12/2018 11:43 | 133.68 | 4.85 | 13.20 |
| 9/12/2018 11:44 | 136.92 | 4.84 | 13.23 |
| 9/12/2018 11:45 | 138.75 | 4.83 | 13.24 |
| Average | 132.54 | 4.87 | 13.19 |

Run 8

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|---------------|-------------|--------------|
| 9/12/2018 12:05 | 133.54 | 4.78 | 13.35 |
| 9/12/2018 12:06 | 133.80 | 4.76 | 13.38 |
| 9/12/2018 12:07 | 133.48 | 4.78 | 13.35 |
| 9/12/2018 12:08 | 133.82 | 4.77 | 13.36 |
| 9/12/2018 12:09 | 134.38 | 4.76 | 13.37 |
| 9/12/2018 12:10 | 135.71 | 4.76 | 13.38 |
| 9/12/2018 12:11 | 133.09 | 4.78 | 13.35 |
| 9/12/2018 12:12 | 132.55 | 4.77 | 13.38 |
| 9/12/2018 12:13 | 133.04 | 4.76 | 13.38 |
| 9/12/2018 12:14 | 132.43 | 4.75 | 13.38 |
| 9/12/2018 12:15 | 133.76 | 4.74 | 13.40 |
| 9/12/2018 12:16 | 134.82 | 4.76 | 13.38 |
| 9/12/2018 12:17 | 134.59 | 4.76 | 13.39 |
| 9/12/2018 12:18 | 135.98 | 4.74 | 13.41 |
| 9/12/2018 12:19 | 133.50 | 4.75 | 13.39 |
| 9/12/2018 12:20 | 133.75 | 4.75 | 13.40 |
| 9/12/2018 12:21 | 131.78 | 4.75 | 13.40 |
| 9/12/2018 12:22 | 130.84 | 4.75 | 13.41 |
| 9/12/2018 12:23 | 130.18 | 4.74 | 13.42 |
| 9/12/2018 12:24 | 131.22 | 4.75 | 13.40 |
| 9/12/2018 12:25 | 131.63 | 4.75 | 13.40 |
| Average | 133.23 | 4.76 | 13.38 |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Run 9

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|---------------|-------------|--------------|
| 9/12/2018 12:45 | 129.66 | 4.72 | 13.45 |
| 9/12/2018 12:46 | 129.84 | 4.72 | 13.44 |
| 9/12/2018 12:47 | 129.59 | 4.71 | 13.47 |
| 9/12/2018 12:48 | 128.25 | 4.72 | 13.46 |
| 9/12/2018 12:49 | 126.63 | 4.71 | 13.46 |
| 9/12/2018 12:50 | 128.26 | 4.70 | 13.48 |
| 9/12/2018 12:51 | 127.51 | 4.71 | 13.47 |
| 9/12/2018 12:52 | 125.83 | 4.71 | 13.47 |
| 9/12/2018 12:53 | 127.05 | 4.69 | 13.49 |
| 9/12/2018 12:54 | 126.97 | 4.70 | 13.48 |
| 9/12/2018 12:55 | 125.73 | 4.71 | 13.47 |
| 9/12/2018 12:56 | 126.08 | 4.70 | 13.49 |
| 9/12/2018 12:57 | 126.19 | 4.70 | 13.47 |
| 9/12/2018 12:58 | 126.13 | 4.70 | 13.48 |
| 9/12/2018 12:59 | 126.93 | 4.69 | 13.50 |
| 9/12/2018 13:00 | 126.00 | 4.69 | 13.50 |
| 9/12/2018 13:01 | 125.54 | 4.72 | 13.46 |
| 9/12/2018 13:02 | 125.58 | 4.69 | 13.50 |
| 9/12/2018 13:03 | 124.92 | 4.71 | 13.50 |
| 9/12/2018 13:04 | 123.62 | 4.71 | 13.48 |
| 9/12/2018 13:05 | 123.69 | 4.69 | 13.50 |
| Average | 126.67 | 4.70 | 13.48 |

Run 10

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|---------------|-------------|--------------|
| 9/12/2018 13:25 | 123.62 | 4.75 | 13.44 |
| 9/12/2018 13:26 | 119.69 | 4.74 | 13.44 |
| 9/12/2018 13:27 | 119.95 | 4.73 | 13.46 |
| 9/12/2018 13:28 | 119.46 | 4.75 | 13.44 |
| 9/12/2018 13:29 | 119.57 | 4.74 | 13.44 |
| 9/12/2018 13:30 | 119.65 | 4.74 | 13.46 |
| 9/12/2018 13:31 | 118.82 | 4.71 | 13.48 |
| 9/12/2018 13:32 | 118.84 | 4.74 | 13.45 |
| 9/12/2018 13:33 | 119.74 | 4.74 | 13.45 |
| 9/12/2018 13:34 | 146.79 | 4.72 | 13.47 |
| 9/12/2018 13:35 | 131.59 | 4.74 | 13.46 |
| 9/12/2018 13:36 | 121.58 | 4.72 | 13.48 |
| 9/12/2018 13:37 | 116.57 | 4.73 | 13.48 |
| 9/12/2018 13:38 | 119.07 | 4.72 | 13.48 |
| 9/12/2018 13:39 | 118.30 | 4.73 | 13.47 |
| 9/12/2018 13:40 | 119.07 | 4.71 | 13.50 |
| 9/12/2018 13:41 | 118.24 | 4.73 | 13.47 |
| 9/12/2018 13:42 | 119.04 | 4.71 | 13.49 |
| 9/12/2018 13:43 | 120.24 | 4.71 | 13.49 |
| 9/12/2018 13:44 | 118.65 | 4.71 | 13.50 |
| 9/12/2018 13:45 | 117.49 | 4.69 | 13.52 |
| Average | 121.24 | 4.73 | 13.47 |



Volumetric Flow Test Run Data Summary

Primary Energy
Cokenergy Facility
HRCC Stack 201

| Operating Level: | High | High | High | High | High | High | High | High | High | High | High | High | High | Average |
|------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Run No.: | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | | |
| Start Date: | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 |
| End Date: | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 |
| Start Time: | 7:15 | 8:00 | 8:40 | 9:20 | 10:00 | 10:45 | 11:25 | 12:05 | 12:45 | 13:25 | | | | |
| End Time: | 7:25 | 8:08 | 8:49 | 9:28 | 10:10 | 10:54 | 11:33 | 12:13 | 12:53 | 13:33 | | | | |

Test Parameters

| | | | | | | | | | | | | | | |
|---|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| P _{bar} - Barometric pressure, inches Hg | 29.26 | 29.28 | 29.28 | 29.28 | 29.28 | 29.31 | 29.28 | 29.28 | 29.26 | 29.26 | 29.26 | 29.26 | 29.26 | 29.28 |
| P _g - Stack Pressure, inches of H2O | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 | -1.00 |
| P _s - Absolute stack pressure, inches Hg | 29.19 | 29.21 | 29.21 | 29.21 | 29.21 | 29.24 | 29.21 | 29.21 | 29.19 | 29.19 | 29.19 | 29.19 | 29.19 | 29.20 |
| T _s - Average stack temperature, °F | 287 | 284 | 285 | 285 | 286 | 286 | 287 | 286 | 286 | 287 | 286 | 286 | 287 | 285.66 |
| % CO ₂ : | 5.2 | 5.1 | 5.1 | 5.0 | 5.0 | 4.9 | 4.9 | 4.8 | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 | 4.94 |
| % O ₂ : | 12.6 | 12.7 | 12.8 | 13.0 | 13.0 | 13.1 | 13.2 | 13.4 | 13.5 | 13.5 | 13.5 | 13.5 | 13.5 | 13.08 |
| % Nitrogen: | 82.2 | 82.2 | 82.1 | 82.0 | 82.0 | 82.0 | 81.9 | 81.8 | 81.8 | 81.8 | 81.8 | 81.8 | 81.8 | 81.98 |
| M _d - dry basis lb/lb mole | 29.336 | 29.324 | 29.328 | 29.320 | 29.320 | 29.308 | 29.312 | 29.304 | 29.292 | 29.292 | 29.292 | 29.292 | 29.292 | 29.31 |
| Stack Diameter, Feet | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 | 18.00 |
| A - Cross Sectional Area of Stack, Ft ² | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 | 254.47 |

Method 2 Results

| | | | | | | | | | | | | | | | |
|--|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Average ΔP | 1.058 | 1.099 | 1.022 | 0.988 | 1.001 | 1.018 | 1.016 | 1.021 | 1.016 | 1.016 | 1.021 | 1.016 | 1.016 | 0.987 | 1.02 |
| Average Sqrt ΔP | 1.027 | 1.047 | 1.010 | 0.993 | 1.000 | 1.008 | 1.007 | 1.010 | 1.007 | 1.007 | 1.010 | 1.007 | 1.007 | 0.992 | 1.01 |
| Bws - Moisture content fraction | 0.138 | 0.145 | 0.140 | 0.137 | 0.140 | 0.135 | 0.140 | 0.132 | 0.136 | 0.136 | 0.132 | 0.136 | 0.136 | 0.141 | 0.14 |
| Mis - wet basis lb/lb mole | 27.772 | 27.679 | 27.738 | 27.771 | 27.736 | 27.779 | 27.734 | 27.807 | 27.755 | 27.755 | 27.807 | 27.755 | 27.755 | 27.75 | 27.75 |
| Average Velocity (ft/sec) | 70.81 | 72.15 | 69.54 | 68.31 | 68.89 | 69.39 | 69.41 | 69.50 | 69.39 | 69.39 | 69.50 | 69.39 | 69.39 | 68.51 | 69.59 |
| Actual cubic feet per minute (ACFM) | 1,081,203 | 1,101,540 | 1,061,759 | 1,043,032 | 1,051,895 | 1,059,431 | 1,059,765 | 1,061,131 | 1,059,436 | 1,059,436 | 1,061,131 | 1,059,436 | 1,059,436 | 1,045,987 | 1,062,518 |
| Standard cubic feet per minute (SCFM) | 745,862 | 763,159 | 734,858 | 721,957 | 727,115 | 733,077 | 731,574 | 733,131 | 731,643 | 731,643 | 733,131 | 731,643 | 731,643 | 721,206 | 734,358 |
| Standard cubic feet per hour (SCFH) | 44,751,720 | 45,789,551 | 44,091,452 | 43,317,420 | 43,626,914 | 43,984,601 | 43,894,446 | 43,987,867 | 43,898,567 | 43,898,567 | 43,987,867 | 43,898,567 | 43,898,567 | 43,272,390 | 44,061,493 |
| Dry Standard cubic feet per minute (DSCFM) | 642,941 | 652,324 | 631,745 | 623,188 | 625,367 | 633,954 | 629,515 | 636,072 | 632,043 | 632,043 | 636,072 | 632,043 | 632,043 | 619,433 | 632,658 |
| Dry Standard cubic feet per hour (DSCFH) | 38,576,474 | 39,139,427 | 37,904,696 | 37,391,290 | 37,522,033 | 38,037,244 | 37,770,914 | 38,164,345 | 37,922,596 | 37,922,596 | 38,164,345 | 37,922,596 | 37,922,596 | 37,165,989 | 37,959,501 |

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 1
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 07:15
End Time: 07:25
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.26
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.19
 T_s - Average stack temperature, °F 287

Gas Molecular Weight Method: % CO₂: 5.2
 Method 3A, Instrumental % O₂: 12.6
 % Nitrogen: 82.2

M_d - dry basis lb/lb mole 29.34
 M_s - wet basis lb/lb mole 27.77

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.138

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 279.000
 Final Meter Volume (cf) 301.456
 Meter Temperature, deg F: 70.9
 Meter Volume Vm(std) (cf): 21.885
 Meter Volume Vw(std) (cf): 3.503
 Delta H: 2.00
 Train Initial Weight, g: 3108.3
 Train Final Weight, g: 3182.6
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.10 | 1.0488 | 286 | 72.25 |
| A | 02 | 1.10 | 1.0488 | 287 | 72.30 |
| A | 03 | 1.10 | 1.0488 | 287 | 72.30 |
| A | 04 | 1.00 | 1.0000 | 286 | 68.89 |
| | | | | | |
| B | 01 | 1.00 | 1.0000 | 287 | 68.94 |
| B | 02 | 0.98 | 0.9899 | 287 | 68.25 |
| B | 03 | 1.00 | 1.0000 | 287 | 68.94 |
| B | 04 | 0.95 | 0.9747 | 286 | 67.15 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 1.10 | 1.0488 | 287 | 72.30 |
| C | 02 | 0.97 | 0.9849 | 286 | 67.85 |
| C | 03 | 0.97 | 0.9849 | 286 | 67.85 |
| C | 04 | 0.95 | 0.9747 | 286 | 67.15 |
| | | | | | |
| D | 01 | 1.20 | 1.0954 | 287 | 75.52 |
| D | 02 | 1.20 | 1.0954 | 287 | 75.52 |
| D | 03 | 1.20 | 1.0954 | 287 | 75.52 |
| D | 04 | 1.10 | 1.0488 | 287 | 72.30 |

Method 2 Results

Average ΔP 1.0575
 Average Sqrt ΔP 1.0275
 Average Velocity (ft/sec) 70.81
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,081,203
 Standard cubic feet per minute (SCFM) 745,862
 Standard cubic feet per hour (SCFH) 44,751,720
 Dry Standard cubic feet per minute (DSCFM) 642,941
 Dry Standard cubic feet per hour (DSCFH) 38,576,474

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 12.0 in. Hg
 Post-Test: 0.000 CFM @ 12.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 2
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 08:00
End Time: 08:08
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.28
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.21
 T_s - Average stack temperature, °F 284

Gas Molecular Weight Method: % CO₂: 5.1
 Method 3A, Instrumental % O₂: 12.7
 % Nitrogen: 82.2

M_d - dry basis lb/lb mole 29.32
 M_s - wet basis lb/lb mole 27.68

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.145

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 301.800
 Final Meter Volume (cf) 324.310
 Meter Temperature, deg F: 75.0
 Meter Volume Vm(std): 21.784
 Meter Volume Vw(std): 3.701
 Delta H: 2.00
 Train Initial Weight, g: 3336.7
 Train Final Weight, g: 3415.2
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.20 | 1.0954 | 284 | 75.47 |
| A | 02 | 1.20 | 1.0954 | 284 | 75.47 |
| A | 03 | 1.20 | 1.0954 | 284 | 75.47 |
| A | 04 | 1.20 | 1.0954 | 283 | 75.42 |
| | | | | | |
| B | 01 | 1.10 | 1.0488 | 285 | 72.30 |
| B | 02 | 1.10 | 1.0488 | 285 | 72.30 |
| B | 03 | 1.10 | 1.0488 | 284 | 72.25 |
| B | 04 | 0.95 | 0.9747 | 284 | 67.15 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 1.00 | 1.0000 | 284 | 68.89 |
| C | 02 | 1.20 | 1.0954 | 284 | 75.47 |
| C | 03 | 1.00 | 1.0000 | 283 | 68.84 |
| C | 04 | 0.84 | 0.9165 | 283 | 63.10 |
| | | | | | |
| D | 01 | 1.20 | 1.0954 | 284 | 75.47 |
| D | 02 | 1.10 | 1.0488 | 284 | 72.25 |
| D | 03 | 1.10 | 1.0488 | 284 | 72.25 |
| D | 04 | 1.10 | 1.0488 | 284 | 72.25 |

Method 2 Results

Average ΔP 1.0994
 Average Sqrt ΔP 1.0473
 Average Velocity (ft/sec) 72.15
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,101,540
 Standard cubic feet per minute (SCFM) 763,159
 Standard cubic feet per hour (SCFH) 45,789,551
 Dry Standard cubic feet per minute (DSCFM) 652,324
 Dry Standard cubic feet per hour (DSCFH) 39,139,427

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 10.0 in. Hg
 Post-Test: 0.000 CFM @ 10.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 3
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 08:40
End Time: 08:49
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.28
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.21
 T_s - Average stack temperature, °F 285

Gas Molecular Weight Method: % CO₂: 5.1
 Method 3A, Instrumental % O₂: 12.8
 % Nitrogen: 82.1

M_d - dry basis lb/lb mole 29.33
 M_s - wet basis lb/lb mole 27.74

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.140

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 324.500
 Final Meter Volume (cf) 347.041
 Meter Temperature, deg F: 80.1
 Meter Volume Vm(std): 21.608
 Meter Volume Vw(std): 3.527
 Delta H: 2.00
 Train Initial Weight, g: 3181.5
 Train Final Weight, g: 3256.3
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.00 | 1.0000 | 285 | 68.86 |
| A | 02 | 1.10 | 1.0488 | 285 | 72.23 |
| A | 03 | 1.10 | 1.0488 | 285 | 72.23 |
| A | 04 | 0.95 | 0.9747 | 285 | 67.12 |
| | | | | | |
| B | 01 | 0.98 | 0.9899 | 285 | 68.17 |
| B | 02 | 0.97 | 0.9849 | 285 | 67.82 |
| B | 03 | 1.00 | 1.0000 | 285 | 68.86 |
| B | 04 | 0.90 | 0.9487 | 285 | 65.33 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 1.10 | 1.0488 | 285 | 72.23 |
| C | 02 | 1.00 | 1.0000 | 285 | 68.86 |
| C | 03 | 1.00 | 1.0000 | 284 | 68.82 |
| C | 04 | 0.88 | 0.9381 | 284 | 64.56 |
| | | | | | |
| D | 01 | 1.10 | 1.0488 | 285 | 72.23 |
| D | 02 | 1.10 | 1.0488 | 284 | 72.18 |
| D | 03 | 1.20 | 1.0954 | 284 | 75.39 |
| D | 04 | 0.97 | 0.9849 | 284 | 67.78 |

Method 2 Results

Average ΔP 1.0219
 Average Sqrt ΔP 1.0100
 Average Velocity (ft/sec) 69.54
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,061,759
 Standard cubic feet per minute (SCFM) 734,858
 Standard cubic feet per hour (SCFH) 44,091,452
 Dry Standard cubic feet per minute (DSCFM) 631,745
 Dry Standard cubic feet per hour (DSCFH) 37,904,696

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 12.0 in. Hg
 Post-Test: 0.000 CFM @ 12.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 4
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 09:20
End Time: 09:28
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.28
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.21
 T_s - Average stack temperature, °F 285

Gas Molecular Weight Method: % CO₂: 5.0
 Method 3A, Instrumental % O₂: 13.0
 % Nitrogen: 82.0

M_d - dry basis lb/lb mole 29.32
 M_s - wet basis lb/lb mole 27.77

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.137

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 347.300
 Final Meter Volume (cf) 370.431
 Meter Temperature, deg F: 81.8
 Meter Volume Vm(std): 22.104
 Meter Volume Vw(std): 3.503
 Delta H: 2.00
 Train Initial Weight, g: 3395.4
 Train Final Weight, g: 3469.7
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.00 | 1.0000 | 285 | 68.82 |
| A | 02 | 1.00 | 1.0000 | 284 | 68.78 |
| A | 03 | 1.10 | 1.0488 | 284 | 72.13 |
| A | 04 | 0.97 | 0.9849 | 284 | 67.74 |
| | | | | | |
| B | 01 | 0.94 | 0.9695 | 285 | 66.73 |
| B | 02 | 1.00 | 1.0000 | 285 | 68.82 |
| B | 03 | 1.00 | 1.0000 | 284 | 68.78 |
| B | 04 | 0.84 | 0.9165 | 284 | 63.04 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 1.00 | 1.0000 | 285 | 68.82 |
| C | 02 | 0.98 | 0.9899 | 285 | 68.13 |
| C | 03 | 0.93 | 0.9644 | 285 | 66.37 |
| C | 04 | 0.84 | 0.9165 | 285 | 63.08 |
| | | | | | |
| D | 01 | 1.10 | 1.0488 | 284 | 72.13 |
| D | 02 | 1.10 | 1.0488 | 285 | 72.18 |
| D | 03 | 1.10 | 1.0488 | 285 | 72.18 |
| D | 04 | 0.90 | 0.9487 | 285 | 65.29 |

Method 2 Results

Average ΔP 0.9875
 Average Sqrt ΔP 0.9929
 Average Velocity (ft/sec) 68.31
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,043,032
 Standard cubic feet per minute (SCFM) 721,957
 Standard cubic feet per hour (SCFH) 43,317,420
 Dry Standard cubic feet per minute (DSCFM) 623,188
 Dry Standard cubic feet per hour (DSCFH) 37,391,290

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 12.0 in. Hg
 Post-Test: 0.000 CFM @ 12.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 5
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 10:00
End Time: 10:10
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.28
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.21
 T_s - Average stack temperature, °F 286

Gas Molecular Weight Method: % CO₂: 5.0
 Method 3A, Instrumental % O₂: 13.0
 % Nitrogen: 82.0

M_d - dry basis lb/lb mole 29.32
 M_s - wet basis lb/lb mole 27.74

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.140

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 370.700
 Final Meter Volume (cf) 393.341
 Meter Temperature, deg F: 81.5
 Meter Volume Vm(std): 21.648
 Meter Volume Vw(std): 3.522
 Delta H: 2.00
 Train Initial Weight, g: 3136.5
 Train Final Weight, g: 3211.2
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.10 | 1.0488 | 286 | 72.28 |
| A | 02 | 1.10 | 1.0488 | 286 | 72.28 |
| A | 03 | 1.10 | 1.0488 | 286 | 72.28 |
| A | 04 | 0.95 | 0.9747 | 286 | 67.17 |
| | | | | | |
| B | 01 | 1.00 | 1.0000 | 286 | 68.91 |
| B | 02 | 1.00 | 1.0000 | 286 | 68.91 |
| B | 03 | 1.00 | 1.0000 | 285 | 68.87 |
| B | 04 | 0.85 | 0.9220 | 285 | 63.49 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 1.00 | 1.0000 | 285 | 68.87 |
| C | 02 | 1.00 | 1.0000 | 285 | 68.87 |
| C | 03 | 1.00 | 1.0000 | 285 | 68.87 |
| C | 04 | 0.90 | 0.9487 | 285 | 65.33 |
| | | | | | |
| D | 01 | 1.00 | 1.0000 | 286 | 68.91 |
| D | 02 | 1.10 | 1.0488 | 286 | 72.28 |
| D | 03 | 1.00 | 1.0000 | 286 | 68.91 |
| D | 04 | 0.92 | 0.9592 | 286 | 66.10 |

Method 2 Results

Average ΔP 1.0013
 Average Sqrt ΔP 1.0000
 Average Velocity (ft/sec) 68.89
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,051,895
 Standard cubic feet per minute (SCFM) 727,115
 Standard cubic feet per hour (SCFH) 43,626,914
 Dry Standard cubic feet per minute (DSCFM) 625,367
 Dry Standard cubic feet per hour (DSCFH) 37,522,033

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass
 Moisture Train:
 Pre-Test: 0.000 CFM @ 13.0 in. Hg
 Post-Test: 0.000 CFM @ 13.0 in. Hg
 Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 6
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 10:45
End Time: 10:54
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.31
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.24
 T_s - Average stack temperature, °F 286

Gas Molecular Weight Method: % CO₂: 4.9
 Method 3A, Instrumental % O₂: 13.1
 % Nitrogen: 82.0

M_d - dry basis lb/lb mole 29.31
 M_s - wet basis lb/lb mole 27.78

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.135

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 393.500
 Final Meter Volume (cf) 416.705
 Meter Temperature, deg F: 80.4
 Meter Volume Vm(std): 22.255
 Meter Volume Vw(std): 3.480
 Delta H: 2.00
 Train Initial Weight, g: 3384.5
 Train Final Weight, g: 3458.3
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.00 | 1.0000 | 286 | 68.82 |
| A | 02 | 1.00 | 1.0000 | 286 | 68.82 |
| A | 03 | 1.10 | 1.0488 | 286 | 72.18 |
| A | 04 | 1.00 | 1.0000 | 286 | 68.82 |
| | | | | | |
| B | 01 | 0.95 | 0.9747 | 285 | 67.04 |
| B | 02 | 0.98 | 0.9899 | 285 | 68.09 |
| B | 03 | 1.10 | 1.0488 | 286 | 72.18 |
| B | 04 | 0.95 | 0.9747 | 286 | 67.08 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 0.95 | 0.9747 | 286 | 67.08 |
| C | 02 | 1.00 | 1.0000 | 286 | 68.82 |
| C | 03 | 1.10 | 1.0488 | 286 | 72.18 |
| C | 04 | 0.89 | 0.9434 | 286 | 64.93 |
| | | | | | |
| D | 01 | 1.10 | 1.0488 | 285 | 72.14 |
| D | 02 | 1.10 | 1.0488 | 285 | 72.14 |
| D | 03 | 1.10 | 1.0488 | 285 | 72.14 |
| D | 04 | 0.97 | 0.9849 | 285 | 67.74 |

Method 2 Results

Average ΔP 1.0181
 Average Sqrt ΔP 1.0084
 Average Velocity (ft/sec) 69.39
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,059,431
 Standard cubic feet per minute (SCFM) 733,077
 Standard cubic feet per hour (SCFH) 43,984,601
 Dry Standard cubic feet per minute (DSCFM) 633,954
 Dry Standard cubic feet per hour (DSCFH) 38,037,244

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 10.0 in. Hg
 Post-Test: 0.000 CFM @ 10.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 7
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 11:25
End Time: 11:33
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.28
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.21
 T_s - Average stack temperature, °F 287

Gas Molecular Weight Method: % CO₂: 4.9
 Method 3A, Instrumental % O₂: 13.2
 % Nitrogen: 81.9

M_d - dry basis lb/lb mole 29.31
 M_s - wet basis lb/lb mole 27.73

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.140

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 416.848
 Final Meter Volume (cf) 439.741
 Meter Temperature, deg F: 79.8
 Meter Volume Vm(std): 21.958
 Meter Volume Vw(std): 3.560
 Delta H: 2.00
 Train Initial Weight, g: 3080.8
 Train Final Weight, g: 3156.3
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.00 | 1.0000 | 287 | 68.96 |
| A | 02 | 1.00 | 1.0000 | 287 | 68.96 |
| A | 03 | 1.10 | 1.0488 | 287 | 72.33 |
| A | 04 | 0.98 | 0.9899 | 287 | 68.27 |
| | | | | | |
| B | 01 | 1.00 | 1.0000 | 287 | 68.96 |
| B | 02 | 1.00 | 1.0000 | 287 | 68.96 |
| B | 03 | 1.00 | 1.0000 | 287 | 68.96 |
| B | 04 | 0.90 | 0.9487 | 287 | 65.42 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 1.00 | 1.0000 | 287 | 68.96 |
| C | 02 | 0.98 | 0.9899 | 287 | 68.27 |
| C | 03 | 0.98 | 0.9899 | 286 | 68.22 |
| C | 04 | 0.83 | 0.9110 | 286 | 62.79 |
| | | | | | |
| D | 01 | 1.10 | 1.0488 | 286 | 72.28 |
| D | 02 | 1.20 | 1.0954 | 286 | 75.49 |
| D | 03 | 1.20 | 1.0954 | 286 | 75.49 |
| D | 04 | 0.98 | 0.9899 | 286 | 68.22 |

Method 2 Results

Average ΔP 1.0156
 Average Sqrt ΔP 1.0068
 Average Velocity (ft/sec) 69.41
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,059,765
 Standard cubic feet per minute (SCFM) 731,574
 Standard cubic feet per hour (SCFH) 43,894,446
 Dry Standard cubic feet per minute (DSCFM) 629,515
 Dry Standard cubic feet per hour (DSCFH) 37,770,914

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 10.0 in. Hg
 Post-Test: 0.000 CFM @ 10.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 8
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 12:05
End Time: 12:13
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.28
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.21
 T_s - Average stack temperature, °F 286

Gas Molecular Weight Method: % CO₂: 4.8
 Method 3A, Instrumental % O₂: 13.4
 % Nitrogen: 81.8

M_d - dry basis lb/lb mole 29.30
 M_s - wet basis lb/lb mole 27.81

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.132

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 439.810
 Final Meter Volume (cf) 462.450
 Meter Temperature, deg F: 82.7
 Meter Volume Vm(std): 21.599
 Meter Volume Vw(std): 3.296
 Delta H: 2.00
 Train Initial Weight, g: 3377.2
 Train Final Weight, g: 3447.1
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.10 | 1.0488 | 286 | 72.18 |
| A | 02 | 1.10 | 1.0488 | 286 | 72.18 |
| A | 03 | 1.10 | 1.0488 | 286 | 72.18 |
| A | 04 | 0.95 | 0.9747 | 286 | 67.08 |
| | | | | | |
| B | 01 | 0.97 | 0.9849 | 286 | 67.78 |
| B | 02 | 0.98 | 0.9899 | 286 | 68.13 |
| B | 03 | 0.97 | 0.9849 | 286 | 67.78 |
| B | 04 | 0.84 | 0.9165 | 286 | 63.08 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 1.10 | 1.0488 | 286 | 72.18 |
| C | 02 | 1.00 | 1.0000 | 286 | 68.82 |
| C | 03 | 1.00 | 1.0000 | 286 | 68.82 |
| C | 04 | 0.93 | 0.9644 | 286 | 66.37 |
| | | | | | |
| D | 01 | 1.10 | 1.0488 | 286 | 72.18 |
| D | 02 | 1.10 | 1.0488 | 286 | 72.18 |
| D | 03 | 1.10 | 1.0488 | 286 | 72.18 |
| D | 04 | 1.00 | 1.0000 | 286 | 68.82 |

Method 2 Results

Average ΔP 1.0213
 Average Sqrt ΔP 1.0098
 Average Velocity (ft/sec) 69.50
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,061,131
 Standard cubic feet per minute (SCFM) 733,131
 Standard cubic feet per hour (SCFH) 43,987,867
 Dry Standard cubic feet per minute (DSCFM) 636,072
 Dry Standard cubic feet per hour (DSCFH) 38,164,345

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 10.0 in. Hg
 Post-Test: 0.000 CFM @ 10.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 9
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 12:45
End Time: 12:53
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.26
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.19
 T_s - Average stack temperature, °F 286

Gas Molecular Weight Method: % CO₂: 4.7
 Method 3A, Instrumental % O₂: 13.5
 % Nitrogen: 81.8

M_d - dry basis lb/lb mole 29.29
 M_s - wet basis lb/lb mole 27.75

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.136

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 462.500
 Final Meter Volume (cf) 485.268
 Meter Temperature, deg F: 85.3
 Meter Volume Vm(std): 21.603
 Meter Volume Vw(std): 3.404
 Delta H: 2.00
 Train Initial Weight, g: 3156.3
 Train Final Weight, g: 3228.5
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.10 | 1.0488 | 286 | 72.28 |
| A | 02 | 1.10 | 1.0488 | 286 | 72.28 |
| A | 03 | 1.10 | 1.0488 | 286 | 72.28 |
| A | 04 | 0.97 | 0.9849 | 285 | 67.83 |
| | | | | | |
| B | 01 | 1.00 | 1.0000 | 285 | 68.87 |
| B | 02 | 1.00 | 1.0000 | 285 | 68.87 |
| B | 03 | 0.97 | 0.9849 | 286 | 67.87 |
| B | 04 | 0.88 | 0.9381 | 286 | 64.65 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 0.97 | 0.9849 | 286 | 67.87 |
| C | 02 | 0.97 | 0.9849 | 286 | 67.87 |
| C | 03 | 1.00 | 1.0000 | 286 | 68.91 |
| C | 04 | 0.92 | 0.9592 | 286 | 66.10 |
| | | | | | |
| D | 01 | 1.00 | 1.0000 | 286 | 68.91 |
| D | 02 | 1.10 | 1.0488 | 286 | 72.28 |
| D | 03 | 1.20 | 1.0954 | 286 | 75.49 |
| D | 04 | 0.97 | 0.9849 | 286 | 67.87 |

Method 2 Results

Average ΔP 1.0156
 Average Sqrt ΔP 1.0070
 Average Velocity (ft/sec) 69.39
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,059,436
 Standard cubic feet per minute (SCFM) 731,643
 Standard cubic feet per hour (SCFH) 43,898,567
 Dry Standard cubic feet per minute (DSCFM) 632,043
 Dry Standard cubic feet per hour (DSCFH) 37,922,596

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 12.0 in. Hg
 Post-Test: 0.000 CFM @ 12.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



METHOD 2 VOLUMETRIC FLOW DATA

Project No: 305091
Company: Primary Energy
Plant: Cokenergy Facility
Unit ID: HRCC
Sample Location: Stack 201
Pitot ID: 888A
Pitot Coefficient: 0.84

Operating Level: High
Run No.: 10
Start Date: 9/12/2018
End Date: 9/12/2018
Start Time: 13:25
End Time: 13:33
RM Testers: RN

Test Parameters

P_{bar} - Barometric pressure, inches Hg 29.26
 P_g - Stack Pressure, inches of H₂O -1.00
 P_s - Absolute stack pressure, inches Hg 29.19
 T_s - Average stack temperature, °F 287

Gas Molecular Weight Method: % CO₂: 4.7
 Method 3A, Instrumental % O₂: 13.5
 % Nitrogen: 81.8

M_d - dry basis lb/lb mole 29.29
 M_s - wet basis lb/lb mole 27.70

Stack Diameter, Feet 18.00
 A - Cross Sectional Area of Stack, Ft² 254.47
B_{ws} - Moisture content fraction 0.141

Moisture Determination

Method Used: 4
 Meter Calibration: 0.997
 Initial Meter Volume (cf) 485.400
 Final Meter Volume (cf) 507.710
 Meter Temperature, deg F: 88.0
 Meter Volume Vm(std): 21.064
 Meter Volume Vw(std): 3.461
 Delta H: 2.00
 Train Initial Weight, g: 3447.1
 Train Final Weight, g: 3520.5
 Condensate Initial Vol, mL: 0.0
 Condensate Final Vol, mL: 0.0

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| A | 01 | 1.00 | 1.0000 | 287 | 69.03 |
| A | 02 | 1.00 | 1.0000 | 287 | 69.03 |
| A | 03 | 1.00 | 1.0000 | 287 | 69.03 |
| A | 04 | 0.95 | 0.9747 | 287 | 67.28 |
| | | | | | |
| B | 01 | 0.98 | 0.9899 | 287 | 68.34 |
| B | 02 | 0.94 | 0.9695 | 287 | 66.93 |
| B | 03 | 0.98 | 0.9899 | 287 | 68.34 |
| B | 04 | 0.85 | 0.9220 | 287 | 63.64 |

| Port | Point | ΔP (in. H ₂ O) | $\sqrt{\Delta P}$ | Temp (°F) | Velocity (V _s) |
|------|-------|--------------------------------------|-------------------|--------------|-------------------------------|
| C | 01 | 0.95 | 0.9747 | 287 | 67.28 |
| C | 02 | 0.98 | 0.9899 | 287 | 68.34 |
| C | 03 | 0.98 | 0.9899 | 287 | 68.34 |
| C | 04 | 0.82 | 0.9055 | 287 | 62.51 |
| | | | | | |
| D | 01 | 1.10 | 1.0488 | 287 | 72.40 |
| D | 02 | 1.10 | 1.0488 | 287 | 72.40 |
| D | 03 | 1.20 | 1.0954 | 287 | 75.62 |
| D | 04 | 0.96 | 0.9798 | 287 | 67.63 |

Method 2 Results

Average ΔP 0.9869
 Average Sqrt ΔP 0.9924
 Average Velocity (ft/sec) 68.51
 No WAF Applied to this Test
 Actual cubic feet per minute (ACFM) 1,045,987
 Standard cubic feet per minute (SCFM) 721,206
 Standard cubic feet per hour (SCFH) 43,272,390
 Dry Standard cubic feet per minute (DSCFM) 619,433
 Dry Standard cubic feet per hour (DSCFH) 37,165,989

Leak Checks:

Pitot: Pre-Test: Pass
 Post-Test: Pass

Moisture Train:
 Pre-Test: 0.000 CFM @ 10.0 in. Hg
 Post-Test: 0.000 CFM @ 10.0 in. Hg

Comments:

Standard conditions of 29.92 in/Hg and 68° F



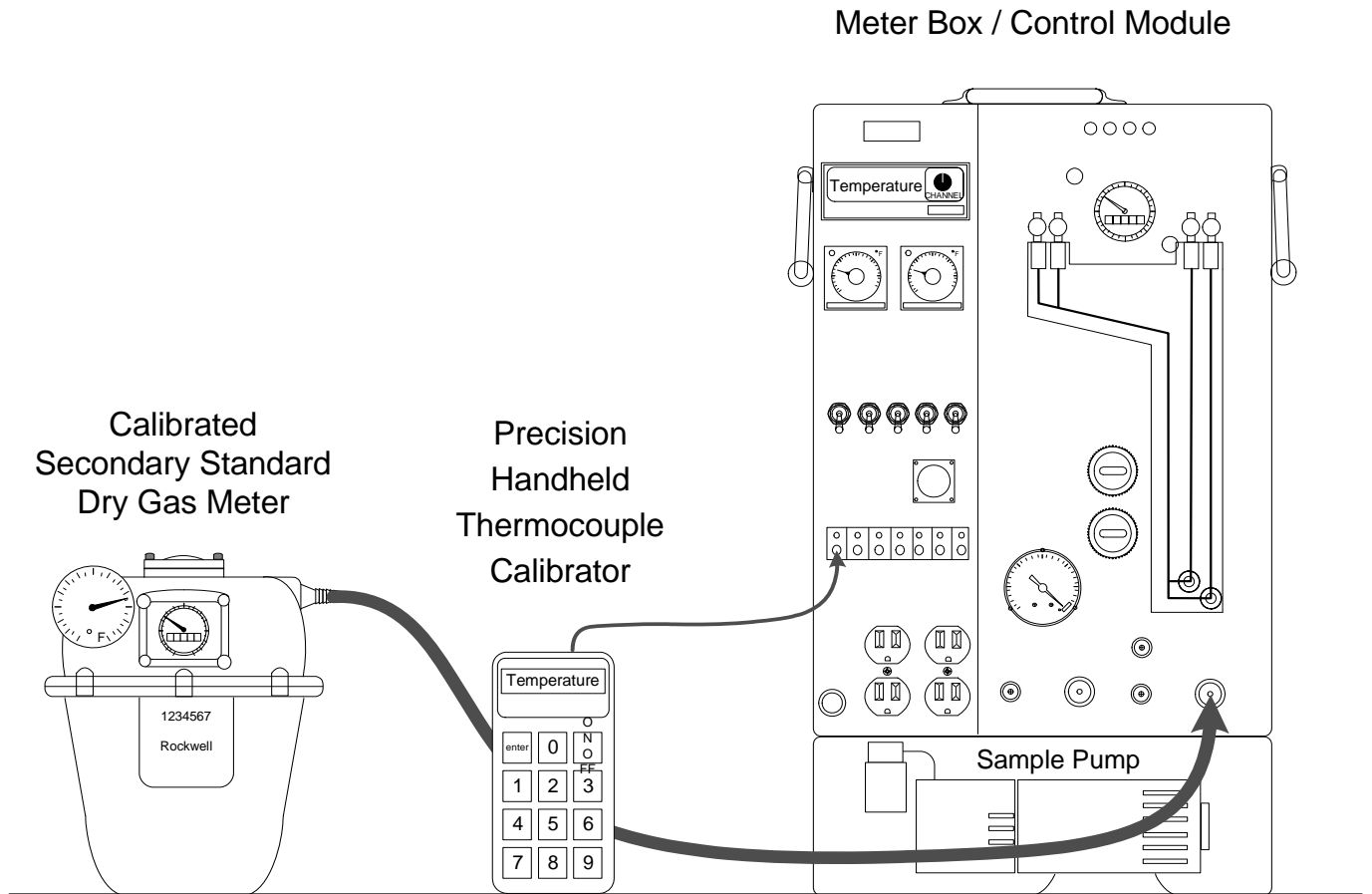
Method 4 Test Run Data Summary

Company: Primary Energy
 Plant: Cokenergy Facility
 Unit: HRCC
 Location: Stack 201

| Test Run Number | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | Average |
|---|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Source Condition | High | High | High | High | High | High | High | High | High | High | |
| Date | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | 9/12/18 | |
| Start Time | 7:15 | 8:00 | 8:40 | 9:20 | 10:00 | 10:45 | 11:25 | 12:05 | 12:45 | 13:25 | |
| End Time | 7:45 | 8:30 | 9:10 | 9:50 | 10:30 | 11:15 | 11:55 | 12:35 | 13:15 | 13:55 | |
| Sample Duration (min): | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |
| Average Stack Temp, T _s (°F): | 286.0 | 285.0 | 285.0 | 285.0 | 286.0 | 287.0 | 287.0 | 286.0 | 286.0 | 287.0 | 286.0 |
| Gas CO ₂ Content (%v/v dry): | 5.2 | 5.1 | 5.1 | 5.0 | 5.0 | 4.9 | 4.9 | 4.8 | 4.7 | 4.7 | 4.9 |
| Gas O ₂ Content (%v/v dry): | 12.6 | 12.7 | 12.8 | 13.0 | 13.0 | 13.1 | 13.2 | 13.4 | 13.5 | 13.5 | 13.1 |
| Gas N ₂ Content (%v/v dry): | 82.2 | 82.2 | 82.1 | 82.0 | 82.0 | 82.0 | 81.9 | 81.8 | 81.8 | 81.8 | 82.0 |
| Gas Dry MW, M _d (lb/lb-mole): | 29.34 | 29.32 | 29.33 | 29.32 | 29.32 | 29.31 | 29.31 | 29.30 | 29.29 | 29.29 | 29.31 |
| Gas Wet MW, M _s (lb/lb-mole): | 27.77 | 27.68 | 27.74 | 27.77 | 27.74 | 27.78 | 27.73 | 27.81 | 27.75 | 27.70 | 27.75 |
| Barometric Pressure, P _{bar} ("Hg) | 29.26 | 29.28 | 29.28 | 29.28 | 29.28 | 29.31 | 29.28 | 29.28 | 29.26 | 29.26 | 29.28 |
| Flue Pressure, P _s ("Hg) | 29.19 | 29.21 | 29.21 | 29.21 | 29.21 | 29.24 | 29.21 | 29.21 | 29.19 | 29.19 | 29.20 |
| Meter Y | 0.997 | 0.997 | 0.997 | 0.997 | 0.997 | 0.997 | 0.997 | 0.997 | 0.997 | 0.997 | 0.997 |
| Meter Pressure, P _m ("H ₂ O): | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Meter Temperature, T _m (°F): | 70.9 | 75.0 | 80.1 | 81.8 | 81.5 | 80.4 | 79.8 | 82.7 | 85.3 | 88.0 | 80.5 |
| Meter Volume, V _m (dcf): | 22.456 | 22.510 | 22.541 | 23.131 | 22.641 | 23.205 | 22.893 | 22.640 | 22.768 | 22.310 | 22.710 |
| Meter Volume, V _m (L): | 635.883 | 637.412 | 638.290 | 654.997 | 641.122 | 657.092 | 648.258 | 641.093 | 644.718 | 631.749 | 643.061 |
| Meter Volume, V _m (dcm): | 0.636 | 0.637 | 0.638 | 0.655 | 0.641 | 0.657 | 0.648 | 0.641 | 0.645 | 0.632 | 0.643 |
| Meter Volume, V _{m(Std)} (dscf): | 21.884 | 21.784 | 21.609 | 22.106 | 21.648 | 22.254 | 21.960 | 21.600 | 21.601 | 21.064 | 21.751 |
| Meter Volume, V _{m(Std)} (dscm): | 0.620 | 0.617 | 0.612 | 0.626 | 0.613 | 0.630 | 0.622 | 0.612 | 0.612 | 0.596 | 0.616 |
| Moisture Volume, V _{wc(Std)} (scf): | 3.503 | 3.701 | 3.527 | 3.503 | 3.522 | 3.480 | 3.560 | 3.296 | 3.404 | 3.461 | 3.496 |
| Fractional Moisture Content, B _{ws} : | 0.138 | 0.145 | 0.140 | 0.137 | 0.140 | 0.135 | 0.139 | 0.132 | 0.136 | 0.141 | 0.138 |

Equipment Configuration for Meter Box Calibration

USEPA Promulgated Method 5





Pre Test DGM Calibration

(before use, as left data)

| | | | |
|--|--|-----------------------------------|--|
| Control Module I.D. No. <u>E44</u> | System Leak Check: <u>Stable @ 8" w.c. @ > 5 min.</u> | Date: <u>03-21-2018</u> | |
| Standard Meter I.D. No.: <u>3623853</u> | Standard Meter Calibration Date: <u>08-04-2017</u> | Calibrated By: <u>L. Campo</u> | |
| Standard Meter (Y _{as}): <u>0.9941</u> | Standard Meter Calibration Due Date: <u>08-04-2018</u> | Barometric Pressure: <u>29.23</u> | |

| Run Number | Orifice Setting in. H ₂ O | | Meter Pressure in. H ₂ O | Standard Meter Volume V _r | Control Module DGM Volume V _d | Standard Meter Temp. F T _r | Dry Gas Meter Inlet Temp. F T _{di} | | Dry Gas Meter Outlet Temp. F T _{do} | | Dry Gas Meter Avg. Temp. F T _d | | Time Min. | Time Sec. | Gamma Correction Coef. Y | Pressure equal to: 0.75 cfm @ STP (DH@) | Flow Rate (Q) scfm |
|--|--------------------------------------|------|-------------------------------------|--------------------------------------|--|---------------------------------------|---|----|--|----|---|----|-----------|-----------|--------------------------|---|--------------------|
| | 1 | 2 | | | | | 1 | 2 | 1 | 2 | 1 | 2 | | | | | |
| Initial | | | | 988.248 | 933.385 | 74 | 74 | 75 | 75 | | | | | | | | |
| Final | | | | 995.554 | 940.698 | 74 | 74 | 76 | 76 | | | | | | | | |
| Difference 1 | 0.35 | 0.35 | | 7.306 | 7.313 | 74 | 74 | 76 | 76 | 76 | 76 | 20 | 2 | 0.995 | | 1.528 | 0.35 |
| Initial | | | | 4.192 | 949.326 | 74 | 74 | 75 | 75 | | | | | | | | |
| Final | | | | 12.444 | 957.550 | 74 | 74 | 76 | 76 | | | | | | | | |
| Difference 2 | 0.85 | 0.85 | | 8.252 | 8.224 | 74 | 74 | 76 | 76 | 76 | 76 | 15 | 5 | 0.998 | | 1.649 | 0.53 |
| Initial | | | | 13.068 | 958.171 | 74 | 74 | 76 | 76 | | | | | | | | |
| Final | | | | 21.254 | 966.327 | 74 | 74 | 76 | 76 | | | | | | | | |
| Difference 3 | 2.00 | 2.00 | | 8.186 | 8.156 | 74 | 74 | 76 | 76 | 76 | 76 | 10 | 20 | 0.996 | | 1.849 | 0.76 |
| Pre Test Calibration Factor (Y_{avg}) | | | | | | | | | | | | | | | | 0.997 | 1.676 |

Specifications: CFR 40, Part 60, Appendix A, Method 5, section 10.3.1. Calibration Before Use.



Pre Test Temperature Indicator Calibration
(For K-Type Thermocouples)

Date: 03-21-2018

Name: L. Campo

Control Module Number: E44

Ambient Temperature: 74 °F

Reference std. thermocouple calibrator: Omega Engineering, Inc. Model No. CL23A *

Reference std. thermocouple calibrator serial number: T-236796

Date of reference std. calibration verification: 6/1/2017

Due date of reference std. calibration verification: 6/1/2018

| Reference Thermometer (°F) | Thermometer Under Test (°F) | Temperature Difference (%) |
|-------------------------------|--------------------------------|-------------------------------|
| 0 | 2 | 0.4 |
| 600 | 602 | 0.2 |
| 1200 | 1201 | 0.1 |

$$\text{Temperature Difference, \%} = \frac{\text{Ref. std. temp. (°F + 460)} - \text{Therm. under test temp. (°F + 460)}}{\text{Reference std temp. (°F + 460)}} \times 100 \leq 1.5 \%$$

* Reference std. is directly traceable to NIST (National Institute of Standards and Technology)



Post Test DGM Calibration

(after use, as found data)

| | | |
|--|--|-----------------------------------|
| Control Module I.D. No. <u>E-44</u> | System Leak Check: <u>Passed @ > 8" w.c. @ > 5 min Date:</u> | 10-09-2018 |
| Standard Meter I.D. No.: <u>3623853</u> | Standard Meter Calibration Date: <u>8-22-2018</u> | Calibrated By: <u>L. Campo</u> |
| Standard Meter (Y _{as}): <u>0.9972</u> | Standard Meter Calibration Due Date: <u>8-22-2019</u> | Barometric Pressure: <u>29.18</u> |

| Run Number | Sample Train Vacuum (Hg") (avg test value) | Sample Train DH@ _{avg} (H ₂ O") (avg test value) | Standard Meter Gas Volume Vr | Control Module DGM Volume Vd | Standard Meter Temp. F Tr | Dry Gas Meter Inlet Temp. F Tdi | | Dry Gas Meter Outlet Temp. F Tdo | | Dry Gas Meter Avg. Temp. F Td | | Time Min. | Time Sec. | Gamma Correction Coef Y | Pressure equal to: 0.75 cfm @ STP (DH@) | Flow Rate (Q) scfm |
|--------------|--|--|------------------------------|------------------------------|---------------------------|---------------------------------|-----|----------------------------------|------|-------------------------------|-------|-----------|-----------|-------------------------|---|--------------------|
| | | | | | | Tdi | Tdo | Td | Min. | Sec. | | | | | | |
| Initial | | | 840.636 | 537.140 | 73 | 74 | 74 | 74 | | | | | | | | |
| Final | | | 848.663 | 545.106 | 73 | 75 | 75 | 75 | | | | | | | | |
| Difference 1 | 0 | 0.85 | 8.027 | 7.966 | 73 | 75 | 75 | 75 | 15 | 16 | 1.006 | | | | 1.785 | 0.50 |
| Initial | | | 848.663 | 545.106 | 73 | 75 | 75 | 75 | | | | | | | | |
| Final | | | 856.667 | 553.042 | 73 | 76 | 76 | 76 | | | | | | | | |
| Difference 2 | 0 | 0.85 | 8.004 | 7.936 | 73 | 76 | 76 | 76 | 15 | 19 | 1.008 | | | | 1.804 | 0.50 |
| Initial | | | 856.667 | 553.042 | 73 | 76 | 76 | 76 | | | | | | | | |
| Final | | | 864.612 | 560.928 | 73 | 77 | 77 | 77 | | | | | | | | |
| Difference 3 | 0 | 0.85 | 7.945 | 7.886 | 73 | 77 | 77 | 77 | 15 | 15 | 1.009 | | | | 1.812 | 0.50 |

| | |
|---|------------|
| Post Test Calibration Factor (Y_{avg}) | 1.008 |
| Pre Test Calibration Factor (Y _{avg}): | 0.997 |
| Pre Test Calibration (Date): | 03-21-2018 |
| % diff. between Pre & Post (Y _{avg}): | 1.1% |

If difference between Pre & Post is less than 5% use Pre Test (Y)

Specifications: CFR 40, Part 60, Appendix A, Method 5, section 10.3.2. Calibration After Use.



Post Test Temperature Indicator Calibration
(For K-Type Thermocouples)

Date: 10-09-2018

Name: L. Campo

Control Module Number: E-44

Ambient Temperature: 73 °F

Reference std. thermocouple calibrator: Omega Engineering, Inc. Model No. CL23A *

Reference std. thermocouple calibrator serial number: T-236796

Date of reference std. calibration verification: 5/31/2018

Due date of reference std. calibration verification: 5/31/2019

| Reference Thermometer (°F) | Thermometer Under Test (°F) | Temperature Difference (%) |
|-------------------------------|--------------------------------|-------------------------------|
| 0 | 1 | 0.2 |
| 600 | 601 | 0.1 |
| 1200 | 1201 | 0.1 |

$$\text{Temperature Difference, \%} = \frac{\text{Ref. std. temp. (°F + 460)} - \text{Therm. under test temp. (°F + 460)}}{\text{Reference std temp. (°F + 460)}} \times 100 \leq 1.5 \%$$

* Reference std. is directly traceable to NIST (National Institute of Standards and Technology)

Field Calibration Tool Identification

| | |
|------------------------|----------------|
| Analyst: | Ryan Novosel |
| Date: | 9/11/2018 |
| Project Number: | 305091 |
| Client: | Primary Energy |
| Test Location: | Stack 201 |

Calibration Tools: Include all of the tools from the field calibration kit that you will be using on this project. (See SOP AM-CAL-025 for instructions on re-verification)

| Item | ID# | S/N | Calibration Due Date |
|--------------------------------|------------|-----------|----------------------|
| Digital Caliper | DC014 | -- | 9/7/2019 |
| Thermometer | TH014 | 122436576 | 9/7/2017 |
| Barometer | BA014 | 160253744 | 3/8/2019 |
| Calibration Weight | W100-014 | 2341 | 9/7/2019 |
| Calibration Weight A | W500-014 | 4593 | 9/7/2019 |
| Calibration Weight B | W500/2-014 | 5094 | 9/7/2019 |
| Type A Angle Finder | AF014 | -- | 9/7/2019 |
| Plastic/Magnetic Torpedo Level | TL014 | -- | -- |

Pre-Test Thermocouple Calibration Checks

| | |
|------------------------|----------------|
| Analyst: | Ryan Novosel |
| Date: | 9/11/18 |
| Project Number: | 305091 |
| Client: | Primary Energy |
| Test Location: | Stack 201 |

(See SOP AM-CAL-005 for instructions)

| | |
|--|--------|
| Console/Meter Box ID # | E44 |
| Probe ID# | 888 |
| Test Location/Measurement Point Info: | Ground |
| NIST Thermometer ID # | TH014 |

Procedure 1: Calibrate thermocouple against a reference thermometer.

After each test run series, check the accuracy (and, hence, the calibration) of each thermocouple system at ambient temperature, or any other temperature, within the range specified by the manufacturer, using a reference thermometer.

Procedure 2: Check the response of the thermocouple to a change in temperature.

Check the "continuity" of the thermocouple by subjecting it to a change in temperature (e.g., removing it from the stack or touching an ice cube). This step will also check for loose connections and reversed connections.

| Measurement | T/C Temp, °F | NIST Thermometer Temp, °F | Difference, °F (± 2) | Continuity Check | Overall Status |
|---------------|--------------|---------------------------|----------------------|------------------|----------------|
| Stack | 80 | 80.5 | 0.5 | Pass | Pass |
| Filter | | | | | |
| Impinger Exit | 79 | 80 | 1.0 | Pass | Pass |
| Meter in | 80 | 80.2 | 0.2 | Pass | Pass |
| Meter Out | 80 | 80.3 | 0.3 | Pass | Pass |
| Probe | | | | | |
| Other | | | | | |
| Other | | | | | |

Notes:

Post-Test Thermocouple Calibration Checks

| | |
|------------------------|----------------|
| Analyst: | Ryan Novosel |
| Date: | 9/13/18 |
| Project Number: | 305091 |
| Client: | Primary Energy |
| Test Location: | Stack 201 |

(See SOP AM-CAL-005 for instructions)

| | |
|--|-----------|
| Console/Meter Box ID # | E44 |
| Probe ID# | 888 |
| Test Location/Measurement Point Info: | Warehouse |
| NIST Thermometer ID # | TH014 |

Procedure 1: Calibrate thermocouple against a reference thermometer.

After each test run series, check the accuracy (and, hence, the calibration) of each thermocouple system at ambient temperature, or any other temperature, within the range specified by the manufacturer, using a reference thermometer.

Procedure 2: Check the response of the thermocouple to a change in temperature.

Check the "continuity" of the thermocouple by subjecting it to a change in temperature (e.g., removing it from the stack or touching an ice cube). This step will also check for loose connections and reversed connections.

| Measurement | T/C Temp, °F | NIST Thermometer Temp, °F | Difference, °F (± 2) | Continuity Check | Overall Status |
|---------------|--------------|---------------------------|----------------------|------------------|----------------|
| Stack | 75 | 75.9 | 0.9 | Pass | Pass |
| Filter | | | | | |
| Impinger Exit | 76 | 76.4 | 0.4 | Pass | Pass |
| Meter in | 76 | 77 | 1.0 | Pass | Pass |
| Meter Out | 76 | 77 | 1.0 | Pass | Pass |
| Probe | | | | | |
| Other | | | | | |
| Other | | | | | |

Notes:

PRE-TEST TYPE S PITOT TUBE INSPECTION

(See SOP AM-CAL-006 for Instructions)

Pitot Tube No. : 888

Date: 9/11/2018

Analyst: Ryan Novosel

Project Number: 305091

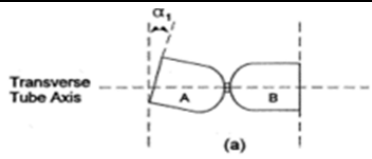
Client: Primary Energy

Test Location: Stack 201

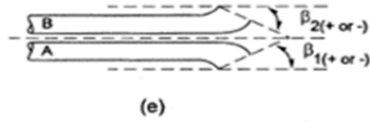
Type S Pitot tube face openings meet alignment specifications illustrated in Figures 2-2 and 2-3 of Method 2?

yes no

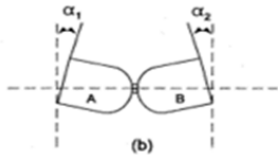
Comments: _____



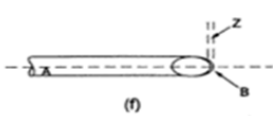
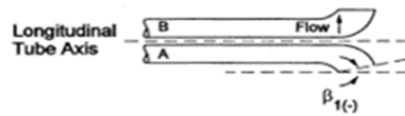
Limit:
 $\alpha_1 < 10^\circ$



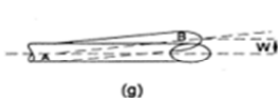
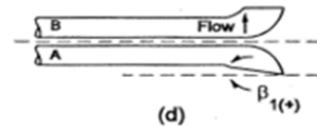
Limit:
 $\beta_1 < 5^\circ$
 $\beta_2 < 5^\circ$



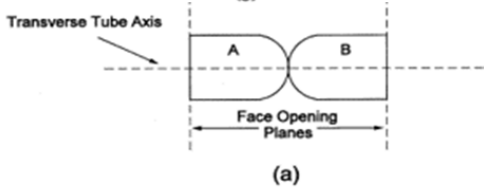
Limit:
 $\alpha_2 < 10^\circ$



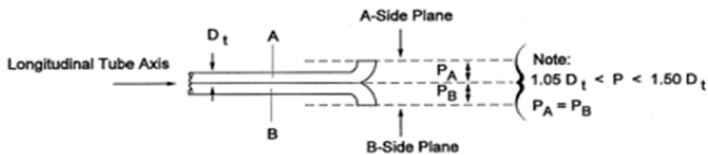
Limit:
 $Z \leq 1/8$ (0.125) inch



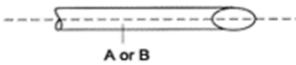
Limit:
 $W \leq 1/32$ (0.0132) inch



Requirement:
Face opening planes perpendicular to transverse axis



Requirement:
Face opening planes parallel to longitudinal axis



Requirement:
Both legs of equal length and centerlines coincident when viewed

POST-TEST TYPE S PITOT TUBE INSPECTION

(See SOP AM-CAL-006 for Instructions)

Pitot Tube No. : 888

Date: 9/13/2018

Analyst: Ryan Novosel

Project Number: 305091

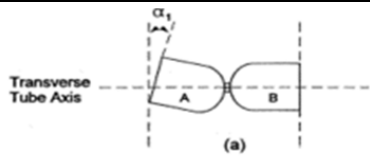
Client: Primary Energy

Test Location: Stack 201

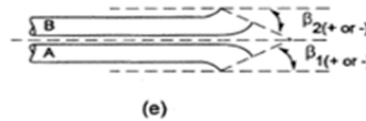
Type S Pitot tube face openings meet alignment specifications illustrated in Figures 2-2 and 2-3 of Method 2?

 yes no

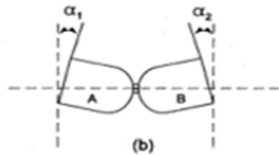
Comments: _____



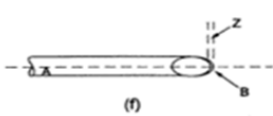
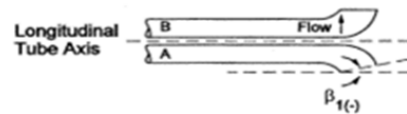
Limit:
 $\alpha_1 < 10^\circ$



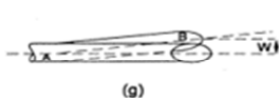
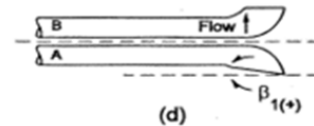
Limit:
 $\beta_1 < 5^\circ$
 $\beta_2 < 5^\circ$



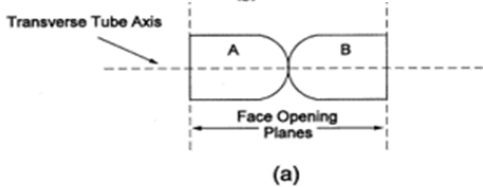
Limit:
 $\alpha_2 < 10^\circ$



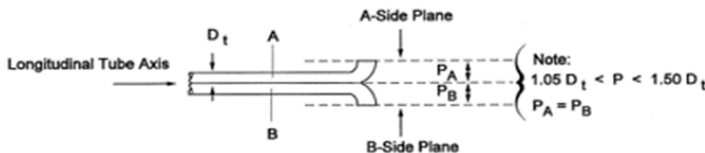
Limit:
 $Z \leq 1/8$ (0.125) inch



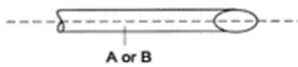
Limit:
 $W \leq 1/32$ (0.0132) inch



Requirement:
Face opening planes perpendicular to transverse axis



Requirement:
Face opening planes parallel to longitudinal axis



Requirement:
Both legs of equal length and centerlines coincident when viewed

PRE-TEST PITOT TUBE ASSEMBLY INSPECTION

Analyst:

Ryan Novosel

Date:

9/11/18

Project Number:

305091

Test Location:

Stack 201

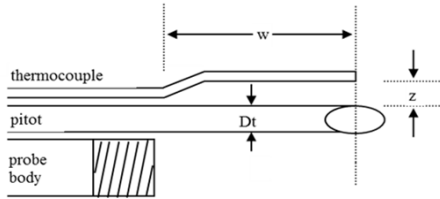
EPA Probe Configuration:

Method 2

Pitot Assembly Intercomponent Spacings Meet Requirements
(See SOP AM-CAL-006 for Instructions)

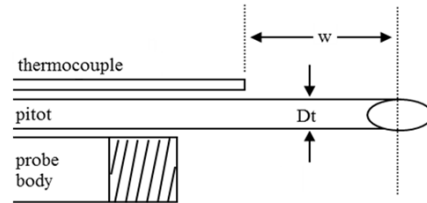
Yes No

Configuration A

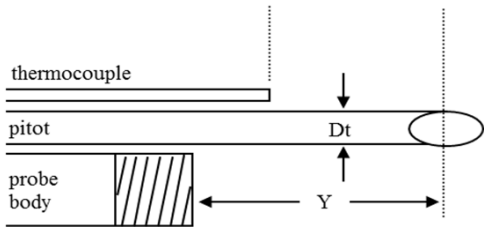


Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$
 $W = \geq 3$ inches
 $Z = \geq 0.75$ inches

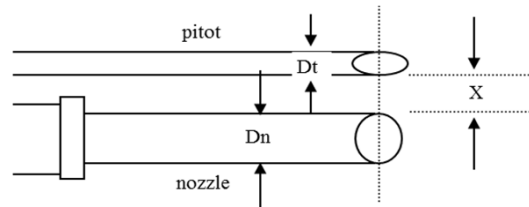
Configuration B



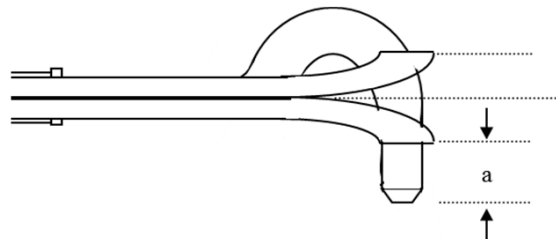
Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$
 $W = \geq 2$ inches



Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$



Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$
 $X = \geq 0.75$ inches



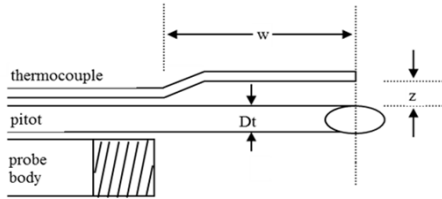
Requirements
 $a = \geq 0$ inches

POST-TEST PITOT TUBE ASSEMBLY INSPECTION

| | |
|---------------------------------|--------------|
| Analyst: | Ryan Novosel |
| Date: | 9/13/18 |
| Project Number: | 305091 |
| Test Location: | Stack 201 |
| EPA Probe Configuration: | Method 2 |

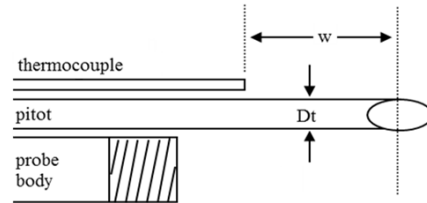
Pitot Assembly Intercomponent Spacings Meet Requirements Yes No
 (See SOP AM-CAL-006 for Instructions)

Configuration A

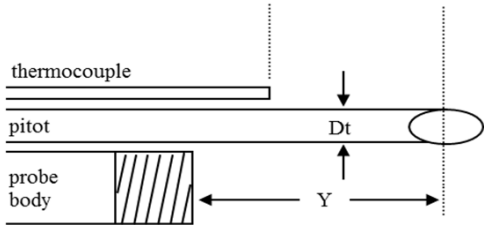


Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$
 $W = \geq 3$ inches
 $Z = \geq 0.75$ inches

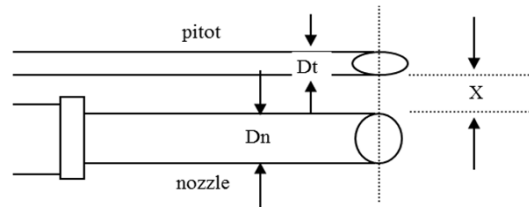
Configuration B



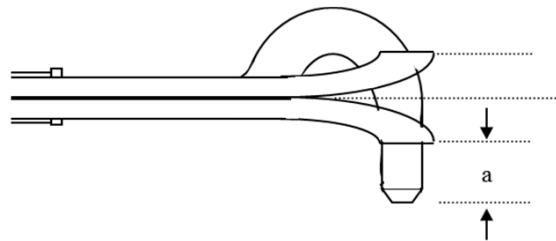
Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$
 $W = \geq 2$ inches



Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$



Requirements
 $D_t = \geq 3/16''$ to $\leq 3/8''$
 $X = \geq 0.75$ inches



Requirements
 $a = \geq 0$ inches



Instrumental Reference Method Field Data

| | | | |
|-----------------------|----------------|--------------|--------------------|
| Project Number: | 305091 | Date: | 9/12/2018 |
| Customer: | Primary Energy | Facility: | Cokenergy Facility |
| Unit Identification: | HRCC | Recorded by: | Gavin Lewis |
| Sample Location: | Stack 201 | Fc Factor: | - |
| Load Level/Condition: | > 50% load | Fd Factor: | - |

| RM Analyzer Information | | | |
|---|--------------|---------|------------------|
| Reference Method Probe Type (Moisture Basis): | | | Extractive (Dry) |
| Pollutant | Manufacturer | Model # | Serial Number |
| NO _x | - | - | - |
| SO ₂ | Thermo | 43C | 509110869 |
| CO | - | - | - |
| CO ₂ | Servomex | 1440 | 01420c/1485 |
| O ₂ | Servomex | 1440 | 01415c/1492 |

| Reference Method Initial Calibration Error Test | | | | | | | | |
|---|---------------|------------------------------|----------|---------------|-------------------|---------------------|-------------|--------------|
| Pollutant | Cal Gas Level | Cal Gas Cylinder Information | | | Analyzer Response | Absolute Difference | % Cal Error | Error Status |
| | | Concentration | Exp Date | ID # | | | | |
| NO _x | Low | - | - | - | - | - | - | - |
| | Mid | - | - | - | - | - | - | - |
| | High | - | - | - | - | - | - | - |
| SO ₂ | Low | 0 | 01/24/26 | EB0041701 | 0.50 | 0.50 | 0.11 | Pass |
| | Mid | 201.8 | 06/13/25 | SG9135799BAL | 202.31 | 0.51 | 0.11 | Pass |
| | High | 452.6 | 01/03/26 | SG9151303 BAL | 456.51 | 3.91 | 0.86 | Pass |
| CO | Low | - | - | - | - | - | - | - |
| | Mid | - | - | - | - | - | - | - |
| | High | - | - | - | - | - | - | - |
| CO ₂ | Low | 0 | 01/24/26 | EB0041701 | 0.03 | 0.03 | 0.17 | Pass |
| | Mid | 8.798 | 05/17/26 | CC473136 | 8.83 | 0.03 | 0.18 | Pass |
| | High | 17.86 | 05/15/23 | CC19838 | 17.86 | 0.00 | 0.00 | Pass |
| O ₂ | Low | 0 | 01/24/26 | EB0041701 | 0.03 | 0.03 | 0.14 | Pass |
| | Mid | 9.976 | 05/17/26 | CC473136 | 10.08 | 0.10 | 0.47 | Pass |
| | High | 22.01 | 05/15/23 | CC19838 | 22.07 | 0.06 | 0.27 | Pass |

| CEM System Information | | | |
|---|--------------------------|---------------|------------------|
| CEM System Probe Type (Moisture Basis): | | | Extractive (Dry) |
| Pollutant | Manufacturer/Model | Serial Number | |
| | | Primary | Backup |
| NO _x | - | - | - |
| SO ₂ | Thermo Scientific 43i-HL | 1152150034 | - |
| CO | - | - | - |
| CO ₂ | - | - | - |
| O ₂ | Brand Gaus 4705 | 11401 | - |



Instrumental Reference Method Field Data

| | | | |
|-----------------------|----------------|--------------|--------------------|
| Project Number: | 305091 | Start Date: | 9/12/2018 |
| Customer: | Primary Energy | End Date: | 9/12/2018 |
| Unit Identification: | HRCC | Facility: | Cokenergy Facility |
| Sample Location: | Stack 201 | Recorded by: | Gavin Lewis |
| Load Level/Condition: | > 50% load | Fc Factor: | - |
| | | Fd Factor: | - |

| Actual Concentration of the Upscale Calibration Gas, C _{MA} | | | | | |
|--|-----------------|-----------------|----|-----------------|----------------|
| | NO _x | SO ₂ | CO | CO ₂ | O ₂ |
| C _{MA} (Day 1) | - | 201.8 | - | 8.798 | 9.976 |
| C _{MA} (Day 2) | - | - | - | - | - |

| System Responses to Zero Calibration Gas | | | | | | | | | | |
|--|-----------------|------|-----------------|------|-----|------|-----------------|------|----------------|------|
| Run No. | NO _x | | SO ₂ | | CO | | CO ₂ | | O ₂ | |
| | Pre | Post | Pre | Post | Pre | Post | Pre | Post | Pre | Post |
| 1 | - | - | 2.29 | 3.50 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 2 | - | - | 3.50 | 4.74 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 3 | - | - | 4.74 | 3.50 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 4 | - | - | 3.50 | 3.42 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 5 | - | - | 3.42 | 4.42 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 6 | - | - | 4.42 | 2.69 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 7 | - | - | 2.69 | 3.42 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 8 | - | - | 3.42 | 3.33 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 9 | - | - | 3.33 | 3.21 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |
| 10 | - | - | 3.21 | 2.25 | - | - | 0.05 | 0.05 | 0.05 | 0.05 |

| System Responses to Upscale Calibration Gas | | | | | | | | | | |
|---|-----------------|------|-----------------|--------|-----|------|-----------------|------|----------------|------|
| Run No. | NO _x | | SO ₂ | | CO | | CO ₂ | | O ₂ | |
| | Pre | Post | Pre | Post | Pre | Post | Pre | Post | Pre | Post |
| 1 | - | - | 197.26 | 196.64 | - | - | 8.76 | 8.77 | 9.98 | 9.98 |
| 2 | - | - | 196.64 | 196.89 | - | - | 8.77 | 8.77 | 9.98 | 9.98 |
| 3 | - | - | 196.89 | 197.72 | - | - | 8.77 | 8.78 | 9.98 | 9.98 |
| 4 | - | - | 197.72 | 198.01 | - | - | 8.78 | 8.77 | 9.98 | 9.98 |
| 5 | - | - | 198.01 | 197.84 | - | - | 8.77 | 8.76 | 9.98 | 9.98 |
| 6 | - | - | 197.84 | 196.75 | - | - | 8.76 | 8.76 | 9.98 | 9.98 |
| 7 | - | - | 196.75 | 197.60 | - | - | 8.76 | 8.76 | 9.98 | 9.98 |
| 8 | - | - | 197.60 | 197.22 | - | - | 8.76 | 8.75 | 9.98 | 9.98 |
| 9 | - | - | 197.22 | 197.39 | - | - | 8.75 | 8.75 | 9.98 | 9.98 |
| 10 | - | - | 197.39 | 196.06 | - | - | 8.75 | 8.73 | 9.98 | 9.98 |



Instrumental Reference Method Calibration Data

| | | | |
|----------------------|----------------|--------------|--------------------|
| Project Number: | 305091 | Start Date: | 9/12/2018 |
| Customer: | Primary Energy | End Date: | 9/12/2018 |
| Unit Identification: | HRCC | Facility: | Cokenergy Facility |
| Sample Location: | Stack 201 | Recorded by: | Gavin Lewis |

SO₂ System Bias/Calibration Error and Drift Summary

| Run # | Calibration Gas Level | Span | Cdir | Initial Values | | Final Values | | Drift (% of span) |
|-------|-----------------------|------------------------------|---------------------------|-----------------------|-------------------------|-----------------------|-------------------------|-------------------|
| | | Span Gas Concentration (ppm) | Direct Cal Response (ppm) | System Response (ppm) | System Bias (% of span) | System Response (ppm) | System Bias (% of span) | |
| 1 | Low Level Gas | 452.6 | 0.5 | 2.29 | 0.4 | 3.50 | 0.7 | 0.3 |
| | Upscale Gas | 452.6 | 202.31 | 197.26 | -1.1 | 196.64 | -1.3 | 0.1 |
| 2 | Low Level Gas | 452.6 | 0.5 | 3.50 | 0.7 | 4.74 | 0.9 | 0.3 |
| | Upscale Gas | 452.6 | 202.31 | 196.64 | -1.3 | 196.89 | -1.2 | 0.1 |
| 3 | Low Level Gas | 452.6 | 0.5 | 4.74 | 0.9 | 3.50 | 0.7 | 0.3 |
| | Upscale Gas | 452.6 | 202.31 | 196.89 | -1.2 | 197.72 | -1.0 | 0.2 |
| 4 | Low Level Gas | 452.6 | 0.5 | 3.50 | 0.7 | 3.42 | 0.6 | 0.0 |
| | Upscale Gas | 452.6 | 202.31 | 197.72 | -1.0 | 198.01 | -1.0 | 0.1 |
| 5 | Low Level Gas | 452.6 | 0.5 | 3.42 | 0.6 | 4.42 | 0.9 | 0.2 |
| | Upscale Gas | 452.6 | 202.31 | 198.01 | -1.0 | 197.84 | -1.0 | 0.0 |
| 6 | Low Level Gas | 452.6 | 0.5 | 4.42 | 0.9 | 2.69 | 0.5 | 0.4 |
| | Upscale Gas | 452.6 | 202.31 | 197.84 | -1.0 | 196.75 | -1.2 | 0.2 |
| 7 | Low Level Gas | 452.6 | 0.5 | 2.69 | 0.5 | 3.42 | 0.6 | 0.2 |
| | Upscale Gas | 452.6 | 202.31 | 196.75 | -1.2 | 197.60 | -1.0 | 0.2 |
| 8 | Low Level Gas | 452.6 | 0.5 | 3.42 | 0.6 | 3.33 | 0.6 | 0.0 |
| | Upscale Gas | 452.6 | 202.31 | 197.60 | -1.0 | 197.22 | -1.1 | 0.1 |
| 9 | Low Level Gas | 452.6 | 0.5 | 3.33 | 0.6 | 3.21 | 0.6 | 0.0 |
| | Upscale Gas | 452.6 | 202.31 | 197.22 | -1.1 | 197.39 | -1.1 | 0.0 |
| 10 | Low Level Gas | 452.6 | 0.5 | 3.21 | 0.6 | 2.25 | 0.4 | 0.2 |
| | Upscale Gas | 452.6 | 202.31 | 197.39 | -1.1 | 196.06 | -1.4 | 0.3 |



Instrumental Reference Method Calibration Data

| | | | |
|----------------------|----------------|--------------|--------------------|
| Project Number: | 305091 | Start Date: | 9/12/2018 |
| Customer: | Primary Energy | End Date: | 9/12/2018 |
| Unit Identification: | HRCC | Facility: | Cokenergy Facility |
| Sample Location: | Stack 201 | Recorded by: | Gavin Lewis |

CO₂ System Bias/Calibration Error and Drift Summary

| Run # | Calibration Gas Level | Span | Cdir | Initial Values | | Final Values | | Drift (% of span) |
|-------|-----------------------|-------------------------------|----------------------------|------------------------|-------------------------|------------------------|-------------------------|-------------------|
| | | Span Gas Concentration (%vol) | Direct Cal Response (%vol) | System Response (%vol) | System Bias (% of span) | System Response (%vol) | System Bias (% of span) | |
| 1 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.76 | -0.4 | 8.77 | -0.3 | 0.1 |
| 2 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.77 | -0.3 | 8.77 | -0.3 | 0.0 |
| 3 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.77 | -0.3 | 8.78 | -0.3 | 0.1 |
| 4 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.78 | -0.3 | 8.77 | -0.3 | 0.1 |
| 5 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.77 | -0.3 | 8.76 | -0.4 | 0.1 |
| 6 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.76 | -0.4 | 8.76 | -0.4 | 0.0 |
| 7 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.76 | -0.4 | 8.76 | -0.4 | 0.0 |
| 8 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.76 | -0.4 | 8.75 | -0.4 | 0.1 |
| 9 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.75 | -0.4 | 8.75 | -0.4 | 0.0 |
| 10 | Low Level Gas | 17.86 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 17.86 | 8.83 | 8.75 | -0.4 | 8.73 | -0.6 | 0.1 |



Instrumental Reference Method Calibration Data

| | | | |
|----------------------|----------------|--------------|--------------------|
| Project Number: | 305091 | Start Date: | 9/12/2018 |
| Customer: | Primary Energy | End Date: | 9/12/2018 |
| Unit Identification: | HRCC | Facility: | Cokenergy Facility |
| Sample Location: | Stack 201 | Recorded by: | Gavin Lewis |

O₂ System Bias/Calibration Error and Drift Summary

| Run # | Calibration Gas Level | Span Gas Concentration (%vol) | Cdir Direct Cal Response (ppm) | Initial Values | | Final Values | | Drift (% of span) |
|-------|-----------------------|-------------------------------|--------------------------------|------------------------|-------------------------|------------------------|-------------------------|-------------------|
| | | | | System Response (%vol) | System Bias (% of span) | System Response (%vol) | System Bias (% of span) | |
| 1 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 2 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 3 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 4 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 5 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 6 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 7 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 8 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 9 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |
| 10 | Low Level Gas | 22.01 | 0.03 | 0.05 | 0.1 | 0.05 | 0.1 | 0.0 |
| | Upscale Gas | 22.01 | 10.08 | 9.98 | -0.5 | 9.98 | -0.5 | 0.0 |



**Instrumental Reference Method
Calibration Corrected Test Data**

Project Number: 305091
 Customer: Primary Energy
 Unit Identification: HRCC
 Sample Location: Stack 201
 RM Probe Type: Extractive (Dry)
 Load Level/Condition: > 50% load

Start Date: 9/12/18
 End Date: 9/12/18
 Facility: Cokenergy Facility
 Recorded by: Gavin Lewis
 Fc Factor: -
 Fd Factor: -

Reference Method Results, As Measured Moisture Basis

| Run # | Date | Start Time | End Time | NOX ppmvd | SO2 ppmvd | CO ppmvd | CO2 % v/v dry | O2 % v/v dry |
|-------|---------|------------|----------|-----------|-----------|----------|---------------|--------------|
| 1 | 9/12/18 | 7:15 | 7:35 | - | 155.5 | - | 5.2 | 12.6 |
| 2 | 9/12/18 | 8:00 | 8:20 | - | 151.7 | - | 5.1 | 12.7 |
| 3 | 9/12/18 | 8:40 | 9:00 | - | 155.5 | - | 5.1 | 12.8 |
| 4 | 9/12/18 | 9:20 | 9:40 | - | 144.9 | - | 5.0 | 13.0 |
| 5 | 9/12/18 | 10:00 | 10:20 | - | 139.3 | - | 5.0 | 13.0 |
| 6 | 9/12/18 | 10:45 | 11:05 | - | 132.6 | - | 4.9 | 13.1 |
| 7 | 9/12/18 | 11:25 | 11:45 | - | 134.6 | - | 4.9 | 13.2 |
| 8 | 9/12/18 | 12:05 | 12:25 | - | 135.1 | - | 4.8 | 13.4 |
| 9 | 9/12/18 | 12:45 | 13:05 | - | 128.3 | - | 4.7 | 13.5 |
| 10 | 9/12/18 | 13:25 | 13:45 | - | 123.3 | - | 4.7 | 13.5 |

Emission Rate Calculation Summary

| Run # | NOX lb/MMBtu | SO2 lb/MMBtu | CO lb/MMBtu | NOX lb/hr | SO2 lb/hr | CO lb/hr | Flow DSCFM |
|-------|--------------|--------------|-------------|-----------|-----------|----------|------------|
| 1 | - | - | - | - | 995.53 | - | 642,941 |
| 2 | - | - | - | - | 985.56 | - | 652,324 |
| 3 | - | - | - | - | 978.42 | - | 631,745 |
| 4 | - | - | - | - | 899.58 | - | 623,188 |
| 5 | - | - | - | - | 867.53 | - | 625,367 |
| 6 | - | - | - | - | 837.47 | - | 633,954 |
| 7 | - | - | - | - | 843.99 | - | 629,515 |
| 8 | - | - | - | - | 855.59 | - | 636,072 |
| 9 | - | - | - | - | 807.91 | - | 632,043 |
| 10 | - | - | - | - | 760.57 | - | 619,433 |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Initial Calibration / Response Time

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry | |
|----------------|-----------|----------|---------|----------------------------|
| 9/12/2018 6:01 | 0.50 | 0.03 | 0.03 | |
| 9/12/2018 6:02 | 0.50 | 0.03 | 0.03 | Local Calibrations |
| 9/12/2018 6:03 | 0.50 | 0.03 | 0.03 | |
| 9/12/2018 6:04 | 0.50 | 0.29 | 0.06 | |
| 9/12/2018 6:05 | 64.21 | 7.24 | 0.07 | |
| 9/12/2018 6:06 | 376.27 | 9.11 | 0.03 | |
| 9/12/2018 6:07 | 433.13 | 9.12 | 0.03 | |
| 9/12/2018 6:08 | 442.89 | 9.13 | 0.03 | |
| 9/12/2018 6:09 | 445.74 | 9.14 | 0.03 | |
| 9/12/2018 6:10 | 446.93 | 9.15 | 0.03 | |
| 9/12/2018 6:11 | 447.85 | 9.15 | 0.03 | |
| 9/12/2018 6:12 | 453.35 | 9.15 | 0.03 | |
| 9/12/2018 6:13 | 455.97 | 9.15 | 0.03 | |
| 9/12/2018 6:14 | 456.51 | 9.15 | 0.03 | |
| 9/12/2018 6:15 | 456.77 | 9.14 | 0.03 | |
| 9/12/2018 6:16 | 291.79 | 8.95 | 0.07 | |
| 9/12/2018 6:17 | 202.31 | 9.13 | 0.03 | |
| 9/12/2018 6:18 | 203.24 | 9.13 | 0.02 | |
| 9/12/2018 6:19 | 202.99 | 9.13 | 0.02 | |
| 9/12/2018 6:20 | 141.18 | 13.53 | 12.09 | |
| 9/12/2018 6:21 | 1.58 | 18.00 | 22.05 | |
| 9/12/2018 6:22 | 1.00 | 17.86 | 22.07 | |
| 9/12/2018 6:23 | 1.00 | 17.85 | 22.08 | |
| 9/12/2018 6:24 | 0.63 | 12.58 | 15.46 | |
| 9/12/2018 6:25 | 0.50 | 8.83 | 10.08 | |
| 9/12/2018 6:26 | 0.50 | 8.84 | 10.08 | |
| 9/12/2018 6:27 | 0.50 | 8.85 | 10.08 | |
| 9/12/2018 6:28 | 1.00 | 4.18 | 15.80 | |
| 9/12/2018 6:29 | 62.05 | 4.24 | 14.08 | |
| 9/12/2018 6:30 | 145.55 | 5.06 | 12.73 | |
| 9/12/2018 6:31 | 146.74 | 5.06 | 12.72 | |
| 9/12/2018 6:32 | 143.71 | 5.06 | 12.72 | |
| 9/12/2018 6:33 | 139.46 | 5.08 | 12.69 | |
| 9/12/2018 6:34 | 140.75 | 5.05 | 12.74 | |
| 9/12/2018 6:35 | 141.90 | 5.08 | 12.70 | |
| 9/12/2018 6:36 | 141.67 | 5.07 | 12.71 | |
| 9/12/2018 6:37 | 143.86 | 5.05 | 12.73 | |
| 9/12/2018 6:38 | 142.88 | 5.08 | 12.68 | |
| 9/12/2018 6:39 | 142.63 | 5.05 | 12.73 | |
| 9/12/2018 6:40 | 143.71 | 5.07 | 12.70 | |
| 9/12/2018 6:41 | 131.04 | 3.32 | 8.19 | |
| 9/12/2018 6:42 | 22.97 | 0.07 | 0.08 | Remote Calibrations |
| 9/12/2018 6:43 | 6.83 | 0.05 | 0.05 | |
| 9/12/2018 6:44 | 3.96 | 0.05 | 0.05 | |
| 9/12/2018 6:45 | 2.96 | 0.05 | 0.05 | |
| 9/12/2018 6:46 | 2.29 | 0.05 | 0.05 | |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Initial Calibration / Response Time

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry | |
|----------------|-----------|----------|---------|---------------------------|
| 9/12/2018 6:47 | 9.73 | 3.32 | 0.04 | SO2 Upscale |
| 9/12/2018 6:48 | 168.58 | 8.88 | 0.03 | |
| 9/12/2018 6:49 | 191.29 | 8.90 | 0.03 | |
| 9/12/2018 6:50 | 195.01 | 8.92 | 0.03 | |
| 9/12/2018 6:51 | 197.26 | 8.93 | 0.03 | SO2 Downscale |
| 9/12/2018 6:52 | 185.51 | 6.16 | 0.03 | |
| 9/12/2018 6:53 | 36.10 | 0.10 | 0.05 | |
| 9/12/2018 6:54 | 8.76 | 0.07 | 0.05 | |
| 9/12/2018 6:55 | 5.19 | 0.05 | 0.05 | |
| 9/12/2018 6:56 | 3.58 | 0.05 | 0.05 | CO2 / O2 Upscale |
| 9/12/2018 6:57 | 2.75 | 0.05 | 0.05 | |
| 9/12/2018 6:58 | 2.19 | 2.95 | 3.38 | |
| 9/12/2018 6:59 | 1.69 | 8.72 | 9.96 | |
| 9/12/2018 7:00 | 1.50 | 8.75 | 9.98 | |
| 9/12/2018 7:01 | 1.50 | 8.76 | 9.99 | |
| 9/12/2018 7:02 | 1.50 | 5.90 | 6.78 | |
| 9/12/2018 7:03 | 1.58 | 0.09 | 0.07 | CO2 / O2 Downscale |
| 9/12/2018 7:04 | 1.42 | 0.07 | 0.05 | |
| 9/12/2018 7:05 | 1.08 | 0.05 | 0.05 | |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Post Calibration Run 1

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|-----------|----------|---------|
| 9/12/2018 7:40 | 3.50 | 0.05 | 0.05 |
| 9/12/2018 7:41 | 58.54 | 6.76 | 0.03 |
| 9/12/2018 7:42 | 185.22 | 8.88 | 0.03 |
| 9/12/2018 7:43 | 194.56 | 8.90 | 0.03 |
| 9/12/2018 7:44 | 196.64 | 8.90 | 0.03 |
| 9/12/2018 7:45 | 124.74 | 8.78 | 7.15 |
| 9/12/2018 7:46 | 13.42 | 8.76 | 9.98 |
| 9/12/2018 7:47 | 5.92 | 8.77 | 9.99 |
| 9/12/2018 7:48 | 4.00 | 8.77 | 10.00 |

Post Calibration Run 2

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|-----------|----------|---------|
| 9/12/2018 8:24 | 4.74 | 0.05 | 0.05 |
| 9/12/2018 8:25 | 54.09 | 6.24 | 0.03 |
| 9/12/2018 8:26 | 185.65 | 8.87 | 0.03 |
| 9/12/2018 8:27 | 195.41 | 8.89 | 0.03 |
| 9/12/2018 8:28 | 196.89 | 8.90 | 0.03 |
| 9/12/2018 8:29 | 127.06 | 8.79 | 6.92 |
| 9/12/2018 8:30 | 13.54 | 8.77 | 9.98 |
| 9/12/2018 8:31 | 6.21 | 8.77 | 10.00 |

Post Calibration Run 3

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|-----------|----------|---------|
| 9/12/2018 9:05 | 3.50 | 0.05 | 0.05 |
| 9/12/2018 9:06 | 53.89 | 6.15 | 0.03 |
| 9/12/2018 9:07 | 183.74 | 8.88 | 0.03 |
| 9/12/2018 9:08 | 195.76 | 8.90 | 0.03 |
| 9/12/2018 9:09 | 197.72 | 8.91 | 0.03 |
| 9/12/2018 9:10 | 125.31 | 8.80 | 7.04 |
| 9/12/2018 9:11 | 13.00 | 8.78 | 9.98 |
| 9/12/2018 9:12 | 6.04 | 8.78 | 10.00 |

Post Calibration Run 4

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|----------------|-----------|----------|---------|
| 9/12/2018 9:45 | 3.42 | 0.05 | 0.05 |
| 9/12/2018 9:46 | 25.05 | 4.58 | 0.04 |
| 9/12/2018 9:47 | 173.09 | 8.86 | 0.03 |
| 9/12/2018 9:48 | 193.94 | 8.89 | 0.03 |
| 9/12/2018 9:49 | 196.33 | 8.90 | 0.03 |
| 9/12/2018 9:50 | 198.01 | 8.91 | 0.03 |
| 9/12/2018 9:51 | 123.73 | 8.78 | 7.42 |
| 9/12/2018 9:52 | 13.34 | 8.77 | 9.98 |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Post Calibration Run 5

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|-----------|----------|---------|
| 9/12/2018 10:29 | 4.42 | 0.05 | 0.05 |
| 9/12/2018 10:30 | 14.51 | 3.43 | 0.04 |
| 9/12/2018 10:31 | 162.16 | 8.85 | 0.03 |
| 9/12/2018 10:32 | 194.14 | 8.89 | 0.03 |
| 9/12/2018 10:33 | 196.31 | 8.90 | 0.03 |
| 9/12/2018 10:34 | 197.84 | 8.90 | 0.03 |
| 9/12/2018 10:35 | 137.85 | 8.80 | 6.44 |
| 9/12/2018 10:36 | 15.59 | 8.76 | 9.98 |
| 9/12/2018 10:37 | 6.73 | 8.76 | 9.98 |

Post Calibration Run 6

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|-----------|----------|---------|
| 9/12/2018 11:12 | 2.69 | 0.05 | 0.05 |
| 9/12/2018 11:13 | 19.35 | 4.20 | 0.04 |
| 9/12/2018 11:14 | 167.86 | 8.85 | 0.03 |
| 9/12/2018 11:15 | 193.81 | 8.88 | 0.03 |
| 9/12/2018 11:16 | 196.75 | 8.89 | 0.03 |
| 9/12/2018 11:17 | 128.08 | 8.78 | 7.30 |
| 9/12/2018 11:18 | 14.42 | 8.75 | 9.98 |
| 9/12/2018 11:19 | 6.50 | 8.76 | 9.98 |

Post Calibration Run 7

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|-----------|----------|---------|
| 9/12/2018 11:50 | 3.42 | 0.05 | 0.05 |
| 9/12/2018 11:51 | 68.30 | 6.41 | 0.03 |
| 9/12/2018 11:52 | 188.05 | 8.88 | 0.03 |
| 9/12/2018 11:53 | 195.10 | 8.90 | 0.03 |
| 9/12/2018 11:54 | 197.60 | 8.90 | 0.03 |
| 9/12/2018 11:55 | 149.79 | 8.81 | 5.21 |
| 9/12/2018 11:56 | 15.29 | 8.76 | 9.97 |
| 9/12/2018 11:57 | 6.39 | 8.76 | 9.98 |

Post Calibration Run 8

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|-----------|----------|---------|
| 9/12/2018 12:30 | 3.33 | 0.05 | 0.05 |
| 9/12/2018 12:31 | 65.89 | 6.40 | 0.03 |
| 9/12/2018 12:32 | 187.64 | 8.85 | 0.03 |
| 9/12/2018 12:33 | 194.95 | 8.88 | 0.03 |
| 9/12/2018 12:34 | 197.22 | 8.88 | 0.03 |
| 9/12/2018 12:35 | 132.72 | 8.78 | 6.97 |
| 9/12/2018 12:36 | 15.93 | 8.75 | 9.96 |
| 9/12/2018 12:37 | 6.33 | 8.75 | 9.98 |

**Primary Energy
Cokenergy Facility
HRCC Stack 201**

Post Calibration Run 9

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|-----------|----------|---------|
| 9/12/2018 13:10 | 3.21 | 0.05 | 0.05 |
| 9/12/2018 13:11 | 60.85 | 6.39 | 0.03 |
| 9/12/2018 13:12 | 186.97 | 8.86 | 0.03 |
| 9/12/2018 13:13 | 195.52 | 8.88 | 0.03 |
| 9/12/2018 13:14 | 197.39 | 8.88 | 0.03 |
| 9/12/2018 13:15 | 125.13 | 8.78 | 7.06 |
| 9/12/2018 13:16 | 11.84 | 8.75 | 9.97 |
| 9/12/2018 13:17 | 5.23 | 8.75 | 9.98 |

Post Calibration Run 10

| Date / Time | SO2 ppmvd | CO2 %dry | O2 %dry |
|-----------------|-----------|----------|---------|
| 9/12/2018 13:51 | 2.25 | 0.05 | 0.05 |
| 9/12/2018 13:52 | 45.49 | 5.20 | 0.03 |
| 9/12/2018 13:53 | 185.64 | 8.84 | 0.03 |
| 9/12/2018 13:54 | 194.45 | 8.87 | 0.03 |
| 9/12/2018 13:55 | 196.06 | 8.88 | 0.03 |
| 9/12/2018 13:56 | 119.00 | 8.75 | 7.48 |
| 9/12/2018 13:57 | 13.00 | 8.73 | 9.97 |
| 9/12/2018 13:58 | 5.17 | 8.73 | 9.98 |



Response Time Verification

| | | | |
|----------------------|----------------|--------------|--------------------|
| Project Number: | 305091 | Test Date: | 9/12/2018 |
| Customer: | Primary Energy | Facility: | Cokenergy Facility |
| Unit Identification: | HRCC | Recorded By: | Gavin Lewis |
| Sample Location: | Stack 201 | | |

| Upscale Response Check | | | | | | | |
|------------------------|---------------|---------------|------------|-----------------|-------------------------|----------------|---------------|
| Pollutant | Cal Gas Level | Cal Gas Conc. | Start Time | Stable Response | Upscale Target Response | Time at Target | Response Time |
| NO _x | - | - | - | - | - | - | - |
| SO ₂ | Mid | 201.80 | 6:47:00 | 197.26 | 187.40 | 6:49:00 | 0:02:00 |
| CO | - | - | - | - | - | - | - |
| CO ₂ | Mid | 8.80 | 6:58:00 | 8.75 | 8.31 | 6:59:00 | 0:01:00 |
| O ₂ | Mid | 9.98 | 6:58:00 | 9.98 | 9.48 | 6:59:00 | 0:01:00 |

Target Response is 95% of the Pre 1 System Response from the Upscale Bias Test

Start time is the time at which gas is introduced upstream of the probe.

Time at target is the time at which the required target response is achieved.

Response time is the difference between the two.

| Downscale Response Check | | | | | | |
|--------------------------|---------------|---------------|------------|---------------------------|----------------|---------------|
| Pollutant | Cal Gas Level | Cal Gas Conc. | Start Time | Downscale Target Response | Time at Target | Response Time |
| NO _x | - | - | - | - | - | - |
| SO ₂ | Mid | 201.80 | 6:52:00 | 10.09 | 6:54:00 | 0:02:00 |
| CO | - | - | - | - | - | - |
| CO ₂ | Mid | 8.80 | 7:02:00 | 0.44 | 7:03:00 | 0:01:00 |
| O ₂ | Mid | 9.98 | 7:02:00 | 0.50 | 7:03:00 | 0:01:00 |

Target Response is 0.5 ppm or 5.0 percent of the upscale gas concentration (whichever is less restrictive)

| System Response Times | |
|-----------------------|---------------|
| Pollutant | Response Time |
| NO _x | 0:00:00 |
| SO ₂ | 0:02:00 |
| CO | 0:00:00 |
| CO ₂ | 0:01:00 |
| O ₂ | 0:01:00 |

System response is the longer of the responses to zero and upscale gas.

ANALYZER INTERFERENCE RESPONSE TEST

USEPA Reference Method: 6C Analyzer Type: SO₂

Analyzer Manufacturer: TECO Model Number: 43C

Date of Test: 2/23/2007

| Test No. | Time | SO ₂ ppm (wet) | | Percent Difference |
|--------------------------|-----------|---------------------------|----------|--------------------|
| | | Method 6C | Method 6 | |
| 1 | 1713-1743 | 92.73 | 92.02 | 0.77 |
| 2 | 1752-1822 | 214.16 | 209.55 | 2.20 |
| 3 | 1919-1949 | 734.74 | 735.69 | -0.13 |
| Total Percent Difference | | | | 2.84 |

Total percent difference allowable is $\leq 7\%$.

Detailed interference response test data is maintained on file and is available upon request.

ANALYZER INTERFERENCE RESPONSE TEST

USEPA Reference Method: 3A Analyzer Type: CO₂

Analyzer Manufacturer: Servomex Model Number: 1440

Analyzer Span: 0-20%

Test Performed by: D. Grabowski Date: 1/23/1998

| Interference Gas | Interference Gas Concentration | Affect of Interference Gas on Analyzer | |
|----------------------|--------------------------------|--|-----------------|
| | | Analyzer Response, ppm | Percent of Span |
| NO _x | 498.0 ppm | -0.02 | -0.10 |
| SO ₂ | 208.9 ppm | -0.02 | -0.10 |
| CO | 450.7 ppm | -0.02 | -0.10 |
| CO ₂ | 10.06% | -- | -- |
| O ₂ | 22.5% | -0.02 | -0.10 |
| Total Response (sum) | | -0.04 | -0.40 |

Total affect on analyzer reading must be < 2% of analyzer span.

Detailed interference response test data is maintained on file and is available upon request.

ANALYZER INTERFERENCE RESPONSE TEST

USEPA Reference Method: 3A Analyzer Type: O₂

Analyzer Manufacturer: Servomex Model Number: 1440

Analyzer Span: 0-25%

Test Performed by: D. Grabowski Date: 1/23/1998

| Interference Gas | Interference Gas Concentration | Affect of Interference Gas on Analyzer | |
|----------------------|--------------------------------|--|-----------------|
| | | Analyzer Response, ppm | Percent of Span |
| NO _x | 498.0 ppm | 0.02 | 0.08 |
| SO ₂ | 208.9 ppm | 0.02 | 0.08 |
| CO | 450.7 ppm | 0.00 | 0.00 |
| CO ₂ | 10.06% | 0.00 | 0.00 |
| O ₂ | 22.5% | -- | -- |
| Total Response (sum) | | 0.04 | 0.16 |

Total affect on analyzer reading must be < 2% of analyzer span.

Detailed interference response test data is maintained on file and is available upon request.

CERTIFICATE OF BATCH ANALYSIS

Grade of Product: CEM-CAL ZERO

| | | | |
|--------------------|----------------------------|--------------------|-----------------|
| Part Number: | NI CZ15A | Reference Number: | 136-401112246-1 |
| Cylinder Analyzed: | CC119441 | Cylinder Volume: | 142.0 CF |
| Laboratory: | 192 - Elk Grove (SAP) - IL | Cylinder Pressure: | 2000 PSIG |
| Analysis Date: | Jan 24, 2018 | Valve Outlet: | 580 |
| Lot Number: | 136-401112246-1 | | |

Expiration Date: Jan 24, 2026

EB0041701

ANALYTICAL RESULTS


| Component | Requested Purity | Certified Concentration |
|-----------------|------------------|-------------------------|
| NITROGEN | 99.9995 % | 99.9995 % |
| CARBON DIOXIDE | < 1.0 PPM | <LDL 0.12 PPM |
| NOx | < 0.1 PPM | < 0.1 PPM |
| SO2 | < 0.1 PPM | < 0.1 PPM |
| THC | < 0.1 PPM | <LDL 0.04 PPM |
| CARBON MONOXIDE | < 0.5 PPM | <LDL 0.12 PPM |

Permanent Notes: Airgas certifies that the contents of this cylinder meet the requirements of 40 CFR 72.2

Cylinders in Batch:

CC119441, CC128062, CC14648, CC214337, CC222236, CC346464, CC401454, CC450417, CC462173, EB0033993, EB0034727, EB0039072, EB0039355, EB0039363, EB0039426, EB0039718, EB0040297, EB0040334, EB0041697, EB0041701

Impurities verified against analytical standards traceable to NIST by weight and/or analysis.



TRC Report 305094
Approved For Release

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

| | | | |
|------------------|------------------------|---------------------|----------------|
| Part Number: | E05NI90E15A8N35 | Reference Number: | 54-124622327-1 |
| Cylinder Number: | SG9135799BAL | Cylinder Volume: | 149.3 CF |
| Laboratory: | 124 - Chicago - IL | Cylinder Pressure: | 2015 PSIG |
| PGVP Number: | B12017 | Valve Outlet: | 660 |
| Gas Code: | CO,CO2,NO,NOX,SO2,BALN | Certification Date: | Jun 13, 2017 |

Expiration Date: Jun 13, 2025

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

| ANALYTICAL RESULTS | | | | | |
|--------------------|-------------------------|----------------------|-----------------|----------------------------|------------------------|
| Component | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
| NOX | 200.0 PPM | 197.7 PPM | G1 | +/- 0.7% NIST Traceable | 06/05/2017, 06/13/2017 |
| CARBON MONOXIDE | 200.0 PPM | 193.9 PPM | G1 | +/- 1.0% NIST Traceable | 06/06/2017 |
| NITRIC OXIDE | 200.0 PPM | 197.7 PPM | G1 | +/- 0.7% NIST Traceable | 06/05/2017, 06/13/2017 |
| SULFUR DIOXIDE | 200.0 PPM | 201.8 PPM | G1 | +/- 0.8% NIST Traceable | 06/05/2017, 06/13/2017 |
| CARBON DIOXIDE | 9.000 % | 8.946 % | G1 | +/- 0.8% NIST Traceable | 06/05/2017 |
| NITROGEN | Balance | | | | |

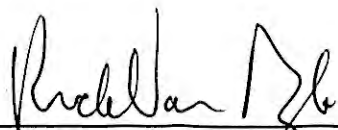
| CALIBRATION STANDARDS | | | | | |
|-----------------------|-----------|-------------|-------------------------------------|-------------|-----------------|
| Type | Lot ID | Cylinder No | Concentration | Uncertainty | Expiration Date |
| NTRM | 14060114 | CC432959 | 990.9 PPM CARBON MONOXIDE/NITROGEN | +/- 0.6% | Nov 18, 2019 |
| PRM | 12312 | 680179 | 10.01 PPM NITROGEN DIOXIDE/NITROGEN | +/- 2.0% | Oct 15, 2014 |
| NTRM | 15060334 | CC448443 | 241 PPM NITRIC OXIDE/NITROGEN | +/- 0.5% | Mar 30, 2021 |
| NTRM | 15060315 | CC448252 | 241.0 PPM NITRIC OXIDE/NITROGEN | +/- 0.5% | Mar 30, 2021 |
| GMIS | 812201405 | CC502159 | 4.861 PPM NITROGEN DIOXIDE/NITROGEN | +/- 2.0% | Aug 12, 2017 |
| NTRM | 15060618 | CC450443 | 248.1 PPM SULFUR DIOXIDE/NITROGEN | +/- 0.6% | Dec 17, 2020 |
| NTRM | 12061356 | CC361031 | 11.002 % CARBON DIOXIDE/NITROGEN | +/- 0.6% | Jan 11, 2018 |

The SRM, PRM or RGM noted above is only in reference to the GMIS used in the assay and not part of the analysis.

| ANALYTICAL EQUIPMENT | | |
|------------------------------|----------------------|-----------------------------|
| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
| Nicolet 6700 AMP0900100 | FTIR | May 22, 2017 |
| CO-1 HORIBA VIA-510 TKPPF7FG | NDIR | May 16, 2017 |
| Nicolet 6700 AMP0900100 | FTIR | May 22, 2017 |
| Nicolet 6700 AMP0900100 | FTIR | May 22, 2017 |
| Nicolet 6700 AMP0900100 | FTIR | May 22, 2017 |

Triad Data Available Upon Request




 Approved for Release
 TRC Report 305091

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

| | | | |
|------------------|--------------------------|---------------------|----------------|
| Part Number: | E05NI90E15A7762 | Reference Number: | 54-401083591-1 |
| Cylinder Number: | SG9151303BAL | Cylinder Volume: | 149.3 CF |
| Laboratory: | 124 - Chicago (SAP) - IL | Cylinder Pressure: | 2015 PSIG |
| PGVP Number: | B12018 | Valve Outlet: | 660 |
| Gas Code: | CO,CO2,NO,NOX,SO2,BALN | Certification Date: | Jan 03, 2018 |

Expiration Date: Jan 03, 2026

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

| ANALYTICAL RESULTS | | | | | |
|--------------------|-------------------------|----------------------|-----------------|----------------------------|------------------------|
| Component | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
| NOX | 450.0 PPM | 460.5 PPM | G1 | +/- 0.7% NIST Traceable | 12/22/2017, 01/03/2018 |
| CARBON MONOXIDE | 450.0 PPM | 444.9 PPM | G1 | +/- 0.9% NIST Traceable | 12/27/2017 |
| NITRIC OXIDE | 450.0 PPM | 460.5 PPM | G1 | +/- 0.7% NIST Traceable | 12/22/2017, 01/03/2018 |
| SULFUR DIOXIDE | 450.0 PPM | 452.6 PPM | G1 | +/- 1.0% NIST Traceable | 12/22/2017, 01/03/2018 |
| CARBON DIOXIDE | 9.000 % | 8.985 % | G1 | +/- 1.0% NIST Traceable | 12/22/2017 |
| NITROGEN | Balance | | | | |

| CALIBRATION STANDARDS | | | | | |
|-----------------------|------------|-------------|-------------------------------------|-------------|-----------------|
| Type | Lot ID | Cylinder No | Concentration | Uncertainty | Expiration Date |
| NTRM | 14060114 | CC432959 | 990.9 PPM CARBON MONOXIDE/NITROGEN | +/- 0.6% | Nov 18, 2019 |
| PRM | 12367 | APEX1099237 | 10.0 PPM NITROGEN DIOXIDE/AIR | +/- 1.5% | Jun 02, 2017 |
| NTRM | 15060416 | CC449822 | 496.8 PPM NITRIC OXIDE/NITROGEN | +/- 0.5% | May 04, 2021 |
| GMIS | 1114201605 | CC506716 | 4.995 PPM NITROGEN DIOXIDE/NITROGEN | +/- 2.0% | Nov 14, 2019 |
| NTRM | 16060130 | CC437452 | 515.2 PPM SULFUR DIOXIDE/NITROGEN | +/- 0.8% | Nov 16, 2021 |
| NTRM | 13060614 | CC413600 | 13.359 % CARBON DIOXIDE/NITROGEN | +/- 0.6% | May 19, 2019 |

The SRM, PRM or RGM noted above is only in reference to the GMIS used in the assay and not part of the analysis.

| ANALYTICAL EQUIPMENT | | |
|----------------------------------|----------------------|-----------------------------|
| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
| Nicolet 6700 AMP0900100 | FTIR | Dec 21, 2017 |
| CO-1 SIEMENS ULTRAMAT 6E N1J5700 | NDIR | Dec 13, 2017 |
| Nicolet 6700 AMP0900100 | FTIR | Dec 21, 2017 |
| Nicolet 6700 AMP0900100 | FTIR | Dec 21, 2017 |
| Nicolet 6700 AMP0900100 | FTIR | Dec 21, 2017 |

Triad Data Available Upon Request



[Handwritten Signature]

Approved for Release

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

| | | | |
|------------------|--------------------------|---------------------|----------------|
| Part Number: | E03NI81E15A37P2 | Reference Number: | 54-401204617-1 |
| Cylinder Number: | CC473136 | Cylinder Volume: | 150.3 CF |
| Laboratory: | 124 - Chicago (SAP) - IL | Cylinder Pressure: | 2015 PSIG |
| PGVP Number: | B12018 | Valve Outlet: | 590 |
| Gas Code: | CO2,O2,BALN | Certification Date: | May 17, 2018 |

Expiration Date: May 17, 2026

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

| ANALYTICAL RESULTS | | | | | |
|--------------------|-------------------------|----------------------|-----------------|----------------------------|-------------|
| Component | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
| CARBON DIOXIDE | 9.000 % | 8.798 % | G1 | +/- 0.8% NIST Traceable | 05/17/2018 |
| OXYGEN | 10.00 % | 9.976 % | G1 | +/- 1.0% NIST Traceable | 05/17/2018 |
| NITROGEN | Balance | | | | |

| CALIBRATION STANDARDS | | | | | |
|-----------------------|----------|-------------|----------------------------------|-------------|-----------------|
| Type | Lot ID | Cylinder No | Concentration | Uncertainty | Expiration Date |
| NTRM | 13060613 | CC413592 | 13.359 % CARBON DIOXIDE/NITROGEN | +/- 0.6% | May 09, 2019 |
| NTRM | 09061430 | CC282477 | 22.53 % OXYGEN/NITROGEN | +/- 0.4% | Mar 08, 2019 |

| ANALYTICAL EQUIPMENT | | |
|-------------------------------|----------------------|-----------------------------|
| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
| CO2-1 HORIBA VIA-510 V1E3H7P5 | NDIR | Apr 24, 2018 |
| O2-1 HORIBA MPA-510 3VUYL9NR | Paramagnetic | Apr 20, 2018 |

Triad Data Available Upon Request



Abbas Hussain

Approved for Release

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

| | | | |
|------------------|--------------------|---------------------|----------------|
| Part Number: | E03NI60E15A1069 | Reference Number: | 54-124493649-4 |
| Cylinder Number: | CC19838 | Cylinder Volume: | 158.2 CF |
| Laboratory: | ASG - Chicago - IL | Cylinder Pressure: | 2015 PSIG |
| PGVP Number: | B12015 | Valve Outlet: | 590 |
| Gas Code: | CO2,O2,BALN | Certification Date: | May 15, 2015 |

Expiration Date: May 15, 2023

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

| ANALYTICAL RESULTS | | | | | |
|--------------------|-------------------------|----------------------|-----------------|----------------------------|-------------|
| Component | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
| CARBON DIOXIDE | 18.00 % | 17.86 % | G1 | +/- 1.1% NIST Traceable | 05/15/2015 |
| OXYGEN | 22.00 % | 22.01 % | G1 | +/- 1.0% NIST Traceable | 05/15/2015 |
| NITROGEN | Balance | | | | |

| CALIBRATION STANDARDS | | | | | |
|-----------------------|----------|-------------|---------------------------------|-------------|-----------------|
| Type | Lot ID | Cylinder No | Concentration | Uncertainty | Expiration Date |
| NTRM | 06120402 | CC184369 | 19.66 % CARBON DIOXIDE/NITROGEN | +/- 0.5% | May 01, 2016 |
| NTRM | 06120204 | CC195893 | 20.90 % OXYGEN/NITROGEN | +/- 0.4% | Dec 01, 2015 |

| ANALYTICAL EQUIPMENT | | |
|-------------------------------|----------------------|-----------------------------|
| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
| CO2-1 HORIBA VIA-510 V1E3H7P5 | NDIR | May 13, 2015 |
| O2-1 HORIBA MPA-510 3VUYL9NR | Paramagnetic | May 11, 2015 |

Triad Data Available Upon Request



Signature on file
Approved for Release



Method 2 Velocity Traverse Data

Project No: 305091
 Company: PRIMARY ENERGY
 Plant: EAST CHICAGO
 Unit ID: (R) BOILER HRCC
 Sample Location: Stack 201

Test Date(s): 9-12-18
 Operating Level: _____
 Recorded by: RN
 Pitot ID: 888
 Pitot Coefficient Cp: .840

Duct Dimensions: _____
 Duct Area (ft²): 254.469
 % CO₂: (1) 5.2 (2) 5.1 (3) 5.1
 % O₂: (1) 12.6 (2) 12.7 (3) 12.8

| Run No: | Time: | P _{bar} ("Hg): | Static ("H ₂ O): |
|-----------------|-------------------------------------|-------------------------|-------------------------------------|
| 1 | 715 - 725 | 29.26 | -1 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.1 | 286 | |
| 2 | 1.1 | 287 | |
| 3 | 1.1 | 287 | |
| 4 | 1.0 | 286 | |
| | | | |
| 2-1 | 1.0 | 287 | |
| 2 | .98 | 287 | |
| 3 | 1.0 | 287 | |
| 4 | .95 | 286 | |
| | | | |
| 3-1 | 1.1 | 287 | |
| 2 | .97 | 286 | |
| 3 | .97 | 286 | |
| 4 | .95 | 286 | |
| | | | |
| 4-1 | 1.2 | 287 | |
| 2 | 1.2 | 287 | |
| 3 | 1.2 | 287 | |
| 4 | 1.1 | 287 | |
| | | | |
| Avg. | | | |
| Leak Check Pre: | <input checked="" type="checkbox"/> | Post: | <input checked="" type="checkbox"/> |

| Run No: | Time: | P _{bar} ("Hg): | Static ("H ₂ O): |
|-----------------|-------------------------------------|-------------------------|-------------------------------------|
| 2 | 800 - 808 | 29.28 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.2 | 284 | |
| 2 | 1.2 | 284 | |
| 3 | 1.2 | 284 | |
| 4 | 1.2 | 283 | |
| | | | |
| 2-1 | 1.1 | 285 | |
| 2 | 1.1 | 285 | |
| 3 | 1.1 | 284 | |
| 4 | .95 | 284 | |
| | | | |
| 3-1 | 1.0 | 284 | |
| 2 | 1.2 | 284 | |
| 3 | 1.0 | 283 | |
| 4 | .84 | 283 | |
| | | | |
| 4-1 | 1.2 | 284 | |
| 2 | 1.1 | 284 | |
| 3 | 1.1 | 284 | |
| 4 | 1.1 | 284 | |
| | | | |
| Avg. | | | |
| Leak Check Pre: | <input checked="" type="checkbox"/> | Post: | <input checked="" type="checkbox"/> |

| Run No: | Time: | P _{bar} ("Hg): | Static ("H ₂ O): |
|-----------------|-------------------------------------|-------------------------|-------------------------------------|
| 3 | 840 - 849 | 29.28 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.0 | 285 | |
| 2 | 1.1 | 285 | |
| 3 | 1.1 | 285 | |
| 4 | .95 | 285 | |
| | | | |
| 2-1 | .95 | 285 | |
| 2 | .97 | 285 | |
| 3 | 1.0 | 285 | |
| 4 | .90 | 285 | |
| | | | |
| 3-1 | 1.1 | 285 | |
| 2 | 1.0 | 285 | |
| 3 | 1.0 | 284 | |
| 4 | .88 | 284 | |
| | | | |
| 4-1 | 1.1 | 285 | |
| 2 | 1.1 | 284 | |
| 3 | 1.2 | 284 | |
| 4 | .87 | 284 | |
| | | | |
| Avg. | | | |
| Leak Check Pre: | <input checked="" type="checkbox"/> | Post: | <input checked="" type="checkbox"/> |

| Moisture Test Data | | | | | | | Field Balance ID: | |
|--------------------|------------------------------------|------------------------|------------------|--------------|------------------|---------------------|---------------------|-----|
| Time | Meter Vol (ft ³ or (L)) | ΔH ("H ₂ O) | Meter Temp. (°F) | Vacuum ("Hg) | Outlet Temp (°F) | Meter ID: Y= | Standard Weight ID: | |
| | | | | | | | Train Weight | |
| | | | | | | Initial | | g |
| | | | | | | Final | | g |
| | | | | | | Gain | | g |
| | | | | | | Moisture Leak Check | | |
| Net | | | | | | Pre | @ | "Hg |
| Avg. | | | | | | Post | @ | "Hg |
| | | | | | | | Comments: | |



Method 2 Velocity Traverse Data

Project No: 305091
 Company: PRIMARY ENERGY
 Plant: EAST CHICAGO
 Unit ID: HRCC
 Sample Location: STACK 201

Test Date(s): 9-12-18
 Operating Level: _____
 Recorded by: RW
 Pitot ID: 888
 Pitot Coefficient Cp: .840

Duct Dimensions: _____
 Duct Area (ft²): 254.469
 % CO₂: (4) 5.0 (5) 5.0 (6) 4.9
 % O₂: (4) 13.0 (5) 13.0 (6) 13.1

| Run No: | Time: | P _{bar} ("Hg): | Static ("H ₂ O): |
|---|----------------------|-------------------------|-----------------------------|
| 4 | 920 - 928 | 27.25 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.0 | 285 | |
| 2 | 1.0 | 284 | |
| 3 | 1.1 | 284 | |
| 4 | .97 | 284 | |
| 2-1 | .94 | 285 | |
| 2 | 1.0 | 285 | |
| 3 | 1.0 | 284 | |
| 4 | .84 | 284 | |
| 3-1 | 1.0 | 285 | |
| 2 | .98 | 285 | |
| 3 | .93 | 285 | |
| 4 | .84 | 285 | |
| 4-1 | 1.1 | 284 | |
| 2 | 1.1 | 285 | |
| 3 | 1.1 | 285 | |
| 4 | .80 | 285 | |
| Avg. <input checked="" type="checkbox"/> | | | |
| Leak Check Pre: <input checked="" type="checkbox"/> Post: <input checked="" type="checkbox"/> | | | |

| Run No: | Time: | P _{bar} ("Hg): | Static ("H ₂ O): |
|---|----------------------|-------------------------|-----------------------------|
| 5 | 1000 - 1010 | 29.28 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.1 | 286 | |
| 2 | 1.1 | 286 | |
| 3 | 1.1 | 286 | |
| 4 | .95 | 286 | |
| 2-1 | 1.0 | 286 | |
| 2 | 1.0 | 286 | |
| 3 | 1.0 | 285 | |
| 4 | .85 | 285 | |
| 3-1 | 1.0 | 285 | |
| 2 | 1.0 | 285 | |
| 3 | 1.0 | 285 | |
| 4 | .90 | 285 | |
| 4-1 | 1.0 | 286 | |
| 2 | 1.1 | 286 | |
| 3 | 1.0 | 286 | |
| 4 | .92 | 286 | |
| Avg. <input checked="" type="checkbox"/> | | | |
| Leak Check Pre: <input checked="" type="checkbox"/> Post: <input checked="" type="checkbox"/> | | | |

| Run No: | Time: | P _{bar} ("Hg): | Static ("H ₂ O): |
|---|----------------------|-------------------------|-----------------------------|
| 6 | 1045 - 1054 | 29.31 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.0 | 286 | |
| 2 | 1.0 | 286 | |
| 3 | 1.1 | 286 | |
| 4 | 1.0 | 286 | |
| 2-1 | .95 | 285 | |
| 2 | .98 | 285 | |
| 3 | 1.1 | 286 | |
| 4 | .95 | 286 | |
| 3-1 | .95 | 286 | |
| 2 | 1.0 | 286 | |
| 3 | 1.1 | 286 | |
| 4 | .89 | 286 | |
| 4-1 | 1.1 | 285 | |
| 2 | 1.1 | 285 | |
| 3 | 1.1 | 285 | |
| 4 | .97 | 285 | |
| Avg. <input checked="" type="checkbox"/> | | | |
| Leak Check Pre: <input checked="" type="checkbox"/> Post: <input checked="" type="checkbox"/> | | | |

| Moisture Test Data | | | | | | | Field Balance ID: | |
|---------------------|------------------------------------|------------------------|------------------|--------------|------------------|--------------|---------------------|----------------|
| Time | Meter Vol (ft ³ or (L)) | ΔH ("H ₂ O) | Meter Temp. (°F) | Vacuum ("Hg) | Outlet Temp (°F) | Meter ID: Y= | Standard Weight ID: | |
| | | | | | | | Train Weight | |
| | | | | | | Initial | g | (g) |
| | | | | | | Final | g | Nominal: _____ |
| | | | | | | Gain | g | Measured _____ |
| Moisture Leak Check | | | | | | | Comments: | |
| Net | | | | | | Pre | @ "Hg | |
| Avg. | | | | | | Post | @ "Hg | |



Method 2 Velocity Traverse Data

Project No: 305091
 Company: Primary Energy
 Plant: East Chicago
 Unit ID: HRCC
 Sample Location: Stack 201

Test Date(s): 9-12-18
 Operating Level: _____
 Recorded by: RN
 Pitot ID: 888
 Pitot Coefficient Cp: .890

Duct Dimensions: _____
 Duct Area (ft²): 254.469
 % CO₂: (7)4.9 (8)4.8 (9)4.7
 % O₂: (7)13.2 (8)13.4 (9)13.5

| Run No: | Time: | P _{bar} ("Hg) | Static ("H ₂ O) |
|---|----------------------|------------------------|----------------------------|
| 7 | 1125 - 1133 | 29.25 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.0 | 287 | |
| 2 | 1.0 | 287 | |
| 3 | 1.1 | 287 | |
| 4 | .98 | 287 | |
| 2-1 | 1.0 | 287 | |
| 2 | 1.0 | 287 | |
| 3 | 1.0 | 287 | |
| 4 | .90 | 287 | |
| 3-1 | 1.0 | 287 | |
| 2 | .95 | 287 | |
| 3 | .98 | 287 | |
| 4 | .83 | 287 | |
| 4-1 | 1.1 | 286 | |
| 2 | 1.2 | 286 | |
| 3 | 1.2 | 286 | |
| 4 | .98 | 286 | |
| Avg. <input checked="" type="checkbox"/> | | | |
| Leak Check Pre: <input checked="" type="checkbox"/> Post: <input checked="" type="checkbox"/> | | | |

| Run No: | Time: | P _{bar} ("Hg) | Static ("H ₂ O) |
|---|----------------------|------------------------|----------------------------|
| 8 | 1205 - 1213 | 29.28 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.1 | 286 | |
| 2 | 1.1 | 286 | |
| 3 | 1.1 | 286 | |
| 4 | .95 | 286 | |
| 2-1 | .97 | 286 | |
| 2 | .98 | 286 | |
| 3 | .97 | 286 | |
| 4 | .84 | 286 | |
| 3-1 | 1.1 | 286 | |
| 2 | 1.0 | 286 | |
| 3 | 1.0 | 286 | |
| 4 | .93 | 286 | |
| 4-1 | 1.1 | 286 | |
| 2 | 1.1 | 286 | |
| 3 | 1.1 | 286 | |
| 4 | 1.0 | 286 | |
| Avg. <input checked="" type="checkbox"/> | | | |
| Leak Check Pre: <input checked="" type="checkbox"/> Post: <input checked="" type="checkbox"/> | | | |

| Run No: | Time: | P _{bar} ("Hg) | Static ("H ₂ O) |
|---|----------------------|------------------------|----------------------------|
| 9 | 1245 - 1253 | 29.26 | -1.0 |
| Port-Point | Δp "H ₂ O | T _s (°F) | a |
| 1-1 | 1.1 | 286 | |
| 2 | 1.1 | 286 | |
| 3 | 1.1 | 286 | |
| 4 | .97 | 285 | |
| 2-1 | 1.0 | 285 | |
| 2 | 1.0 | 285 | |
| 3 | .97 | 286 | |
| 4 | .88 | 285 | |
| 3-1 | .97 | 286 | |
| 2 | .97 | 286 | |
| 3 | 1.0 | 285 | |
| 4 | .92 | 285 | |
| 4-1 | 1.0 | 286 | |
| 2 | 1.1 | 286 | |
| 3 | 1.2 | 286 | |
| 4 | .97 | 286 | |
| Avg. <input checked="" type="checkbox"/> | | | |
| Leak Check Pre: <input checked="" type="checkbox"/> Post: <input checked="" type="checkbox"/> | | | |

| Moisture Test Data | | | | | | | Field Balance ID: | |
|--------------------|------------------------------------|------------------------|------------------|--------------|------------------|---------------------|---------------------|-----|
| Time | Meter Vol (ft ³ or (L)) | ΔH ("H ₂ O) | Meter Temp. (°F) | Vacuum ("Hg) | Outlet Temp (°F) | Meter ID: Y= | Standard Weight ID: | |
| | | | | | | ΔH@I: | Train Weight | |
| | | | | | | | Initial | g |
| | | | | | | | Final | g |
| | | | | | | | Gain | g |
| | | | | | | Moisture Leak Check | | |
| Net | | | | | | Pre | @ | "Hg |
| Avg. | | | | | | Post | @ | "Hg |
| | | | | | | | Nominal: _____ | |
| | | | | | | | Measured _____ | |
| | | | | | | | Comments: | |

Moisture Test Run Data

Company: PRIMARY ENERGY
 Plant: EAST CHICAGO
 Unit ID: HRCC
 Location: STACK 201

Project #: 305091
 Test Method: 4
 Test Run #: 5
 Test Date(s): 9-12-18

Console Operator: RN
 Console ID: E44
 Meter Y: .997
 Orifice ΔH@i: 1.676

Unit Operating Mode:

Barometric Pressure ("Hg): 29.28

Static Pressure ("H₂O): -1.0

Pre Leak Check: 0 @ 13

Post Leak Check: 0 @ 13

| Port & Point ID | Clock Time | Dry Gas Meter | | | | | | | Stack (°F) |
|-----------------|------------|----------------------------|------------------------------|------------|-------------|--------------|----------------------|-----|------------|
| | | Volume Liters / Cubic Feet | Pressure ("H ₂ O) | Inlet (°F) | Outlet (°F) | Vacuum ("Hg) | Impinger Outlet (°F) | | |
| 1-1 | 1000 | 370.70 | 2.0 | 83 | 81 | 2 | 59 | 286 | |
| | 1005 | 374.50 | 2.0 | 83 | 81 | 2 | 60 | | |
| | 1010 | 378.29 | 2.0 | 84 | 81 | 2 | 60 | | |
| | 1015 | 382.06 | 2.0 | 82 | 80 | 2 | 61 | | |
| | 1020 | 385.85 | 2.0 | 82 | 80 | 2 | 61 | | |
| | 1025 | 389.60 | 2.0 | 81 | 80 | 2 | 62 | | |
| | 1030 | 393.341 | | | | | | | |
| Net Volume: | | | | | | | | | |
| Average: | | | | | | | | | |

| Moisture Data | | |
|---------------|------------------|-------------------|
| Impinger ID | Tare wt. (grams) | Final wt. (grams) |
| | 3136.5 | 3211.2 |
| Net: | | 74.7 |

Pump/Orifice* Leak Check: Pass Fail / N/A

| Gas Analysis (%v/v dry) | |
|-------------------------|-----------------|
| O ₂ | CO ₂ |
| | |
| | |
| | |
| Average: | |

Comments:

*Required for ALT-009 Meter Calibration Checks

